

# Interior Exploration Using Seismic Investigations, Geodesy, and Heat Transport (InSight) Mission

## **Instrument Deployment Arm (IDA)**

# PDS Archive Software Interface Specification

Rev. 3.3 December 21, 2020

## Prepared by

Susan Slavney, PDS Geosciences Node, Washington University in St. Louis, susan.slavney@wustl.edu

Hallie Abarca, InSight MIPL System Engineer, JPL, hallie.e.gengl@jpl.nasa.gov

Eloise Marteau, InSight IDA Investigation Scientist, JPL, eloise.marteau@jpl.nasa.gov

Grace Lim, Payam Zamani, Galen Hollins, Nythi Udomkesmalee, Cristina De Cesare, Anna Waldron, JPL

## InSight Instrument Deployment Arm

## PDS Archive Software Interface Specification

## Rev. 3.3 December 21, 2020

| Custodians: |  |      |
|-------------|--|------|
|             | Hallie Abarca  | Date |
|             | InSight MIPL System Engineer                               |      |
|             | Eloise Marteau<br>InSight IDA Investigation Scientist      | Date |
| Approved:   |  |      |
|             |  |      |
|             | Ashitey Trebi-Ollenu<br>InSight IDA Principal Investigator | Date |
|             | Raymond E. Arvidson PDS Geosciences Node Manager           | Date |

#### TABLE OF CONTENTS

| 1. INTE    | RODUCTION  | 1  |
|------------|--|----|
| 1.1        | DOCUMENT CHANGE LOG                                      | 1  |
| 1.2        | TBD ITEMS  |    |
| 1.3        | ABBREVIATIONS  |    |
| 1.4        | GLOSSARY   |    |
|            | RVIEW  |    |
|            |  |    |
| 2.1        | PURPOSE AND SCOPE  |    |
| 2.2        | CONTENTS   |    |
| 2.3        | APPLICABLE DOCUMENTS                                     |    |
| 2.4<br>2.5 | AUDIENCE   |    |
| 2.5        | IDA DESCRIPTION  |    |
|            | 6.1 IDA overview   |    |
|            | 6.2 IDA operations                                       |    |
|            | 6.3 IDA calibration                                      |    |
|            |  |    |
|            | DATA PRODUCTS  |    |
| 3.1        | Data Product Overview                                    |    |
| 3.2        | Data Processing  |    |
|            | 2.1 Data Processing Level                                |    |
|            | 2.2 Data Product Generation                              |    |
|            | 2.3 Data Flow  |    |
| 3.3        | STANDARDS USED IN GENERATING DATA PRODUCTS               |    |
|            | 3.1 Time Standards                                       |    |
|            | 3.2 Coordinate Systems                                   |    |
|            | 3.3 Data Storage Conventions                             |    |
| 3.4        | APPLICABLE SOFTWARE                                      |    |
| 3.5        | BACKUPS AND DUPLICATES                                   |    |
| 4. IDA     | ARCHIVE ORGANIZATION, IDENTIFIERS AND NAMING CONVENTIONS | 21 |
| 4.1        | LOGICAL IDENTIFIERS                                      | 21 |
| 4.         | 1.1 LID Formation  | 21 |
| 4.         | 1.2 VID Formation  | 22 |
| 4.         | 1.3 File Naming Conventions                              |    |
| 4.2        | IDA BUNDLES  |    |
| 4.3        | IDA COLLECTIONS  |    |
| 4.4        | IDA Products   |    |
| 4.5        | InSight Document Bundle and Collections                  | 24 |
| 5. IDA     | ARCHIVE PRODUCT FORMATS                                  | 26 |
| 5.1        | Data Product Formats                                     | 26 |
| 5.         | 1.1 IDA Status   | 26 |
| 5.         | 1,2 IDA History  | 29 |
| 5.         | 1.3 IDA Parameters                                       | 29 |
|            | 1.4 IDA Position in Spacecraft Coordinates               |    |
|            | 1.5 Engineering/Science High Priority (SciHi) Data       |    |
|            | 1.6 Engineering/Science Low Priority (SciLo) Data        |    |
| 5.         | 1.7 RSVP Replay MP4                                      |    |
| 5.2        | DOCUMENT PRODUCT FORMATS                                 |    |
| 5.3        | PDS LABEL  | 55 |
| APPEN      | NDIX A – SUPPORT STAFF AND COGNIZANT PERSONS             | 56 |
| APPEN      | NDIX B – IDA DENAVIT-HARTENBERG LINK FRAMES              | 57 |

| APPENDIX C – STRUCTURE OF THE IDA SCIENCE BLOCK        | 58 |
|--|----|
| APPENDIX D – END EFFECTOR FORCES MODEL                 | 59 |
| APPENDIX E – EXAMPLE PDS LABEL FOR AN IDA DATA PRODUCT | 61 |

## LIST OF FIGURES

| Figure 1 - InSight lander with instrument and IDA elements labeled                    | 7  |
|---|----|
| Figure 2 - IDA on the lander deck   |    |
| Figure 3 - End-effector grapple with fingers closed (left) and fingers opened (right) |    |
| Figure 4 - End-effector scoop   |    |
| Figure 5 - End-effector IDC with dust cover opened                                    |    |
| Figure 6 - IDA Frame and Site (local level) Frame                                     |    |
| Figure 7 - IDA, SEIS ASM, and SEIS Grapple Hook Coordinate Frames                     |    |
| Figure 8 - Motor Temperature Model  |    |
| LIST OF TABLES  |    |
|   |    |
| Table 1 - Document Change Log   |    |
| Table 2 - List of TBD items   |    |
| Table 3 - Abbreviations and their meanings  |    |
| Table 4 - IDA data products overview  |    |
| Table 5 - Data Processing Level Definitions   |    |
| Table 6 - IDA telemetry data processed by MIPL  |    |
| Table 7 - Coordinate Frames Used for Surface Operations                               |    |
| Table 8 - File Naming Convention  |    |
| Table 9 - IDA Bundle  |    |
| Table 10 - Collections in the IDA Bundle  |    |
| Table 11 - Collections in the InSight Document Bundle                                 |    |
| Table 12 - Science data parameters  |    |
| Table 13 - Bit-mapped status word   |    |
| Table 14 - Selected tool  |    |
| Table 15 - Grapple phase  |    |
| Table 16 - Archive Support Staff and Cognizant Persons                                | 56 |

## 1. INTRODUCTION

This software interface specification (SIS) describes the format and content of the Instrument Deployment Arm (IDA) Planetary Data System (PDS) data archive. It includes descriptions of the data products and associated metadata, and the archive format, content, and generation pipeline.

## 1.1 Document Change Log

**Table 1 - Document Change Log** 

| DATE       | SECTIONS CHANGED  | REVISION |
|------------|---|----------|
| 2014-04-23 | All   | V0.0     |
| 2015-04-06 | All   | V0.3     |
| 2017-06-07 | Section 2, inputs provided by Khaled Ali  | V0.4     |
| 2017-12-04 | 6.3: Changed description for Coordinated Frame Origin   | V1.1     |
| 2019-01-08 | TBD Items; Acronyms; 1.3: Applicable Documents, 3.3 Data Validation; 4.2 Label and Header Descriptions; 6.2 Time Standards; 7. IDS Archive Organization (new); 8.2 Applicable PDS Software Tools; plus marginal comments throughout | V1.2     |
| 2019-02-27 | RDR added to title; 5.0 section title changed to PDS Data Product Specifications; text added to 5.2, 5.3, and 5.4 to clarify which products go to PDS   | V1.2     |
| 2019-05-31 | Extensive updates throughout the document   | V2.0     |
| 2019-09-12 | Revisions after peer review   | V2.2     |
| 2020-05-11 | Section 5.4.1 updated   | V3.1     |
| 2020-09-10 | 5.1.4. IDA Position in Spacecraft coordinates (new); 5.1.5<br>Description of IDA calibration algorithms   | V3.2     |
| 2020-12-21 | Appendix D – End effector forces model  | V3.3     |

## 1.2 TBD Items

Table 2 - List of TBD items

| Section     | Item                              | Who            |
|-------------|-----------------------------------|----------------|
| Section 2.3 | Soil Mechanics Calibration Report | Eloise Marteau |

## 1.3 Abbreviations

Table 3 - Abbreviations and their meanings

| Abbreviation | Meaning           |
|--------------|-------------------|
| A/D          | Analog-to-Digital |

| AMMOS           | A drawn and Mustei Minnian On soutions Secretary                          |
|-----------------|---|
| AMMOS           | Advanced Multi-Mission Operations System                                  |
| APID            | Application Identifier  |
| APPS            | AMMOS-PDS Pipeline Service  |
| APSS            | Auxiliary Payload Sensor Subsystem  |
| ASCII           | American Standard Code for Information Interchange                        |
| CCSDS           | Consultative Committee for Space Data Systems                             |
| C&DH            | Command and Data Handling   |
| DEM             | Digital Elevation Model   |
| DH              | Denavit and Hartenberg  |
| DSN             | Deep Space Network  |
| EDR             | Experiment Data Record  |
| FOV             | Field of View   |
| FSW             | Flight Software   |
| GDS             | Ground Data System  |
| НОР             | High Input Paraffin   |
| HP <sup>3</sup> | Heat Flow and Physical Properties Package                                 |
| ICC             | InSight Context Camera  |
| IDC             | InSight Deployment Camera   |
| IDA             | InSight Deployment Arm  |
| IDPH            | Image Data Product Header   |
| IDS             | InSight Deployment System   |
| IPIC            | InSight Payload Interface Card  |
| JPL             | Jet Propulsion Laboratory   |
| LID             | Logical Identifier  |
| LIDVID          | Versioned Logical Identifier (logical identifier with version identifier) |
| LSA             | Load Shunt Assembly   |
| LSB             | Least Significant Byte  |
| MC              | Motor Controller  |
| MGA             | Medium Gain Antenna   |
| MIPL            | Multimission Instrument Processing Lab                                    |
| N/A             | Not Applicable  |
| NASA            | National Aeronautics and Space Administration                             |
| NSSDC           | National Space Science Data Center  |
| NSYT            | Acronym for the "InSight" project   |
| PDS             | Planetary Data System   |
| PDS4            | Planetary Data System Version 4   |
| PEB             | Payload Electronics Box   |
|                 | 1 -   |

| RA    | Robotic Arm  |
|-------|--|
| RAE   | Robotic Arm Electronics                                  |
| RDR   | Reduced Data Record                                      |
| RISE  | Rotational and Interior Structure Experiment             |
| RSVP  | Rover Sequencing and Visualization Program               |
| SCLK  | Spacecraft Clock   |
| SEIS  | Seismic Experiment for Investigating the Subsurface      |
| SFDU  | Standard Format Data Unit                                |
| SIS   | Software Interface Specification                         |
| SOL   | Mars Solar day   |
| SPEX  | Spectropolarimeter for Planetary Exploration             |
| SPICE | Spacecraft, Planet, Instrument, C-matrix, Events kernels |
| TBD   | To Be Determined/Defined                                 |
| TBPB  | To Be Provided By  |
| TDS   | Telemetry Delivery Subsystem                             |
| TWINS | Temperature and Wind for InSight                         |
| UHF   | Ultra High Frequency                                     |
| UTC   | Coordinated Universal Time                               |
| VICAR | Video Image Communication and Retrieval                  |
| VID   | Version Identifier                                       |
| WTS   | SEIS wind and temperature shield                         |
| XML   | Extensible Markup Language                               |

## 1.4 Glossary

Many of these definitions are taken from Appendix A of the PDS4 (Planetary Data System Version 4) Concepts Document, <a href="mailto:pds.nasa.gov/pds4/doc/concepts">pds.nasa.gov/pds4/doc/concepts</a>. The reader is referred to that document for more information.

**Archive** – A place in which public records or historical documents are preserved; also the material preserved, often used in plural. The term may be capitalized when referring to all of PDS holdings (i.e., the PDS Archive).

**Basic Product** – The simplest product in PDS4; one or more data objects (and their description objects), which constitute (typically) a single observation, document, etc. The only PDS4 products that are *not* basic products are collection and bundle products.

**Bundle** – A list of related collections. For example, a bundle could list a collection of raw data obtained by an instrument during its mission lifetime, a collection of the calibration products associated with the instrument, and a collection of all documentation relevant to the first two collections.

Class – The set of attributes (including a name and identifier) which describes an item defined in the PDS Information Model. A class is generic, i.e., a template from which individual items may be constructed.

**Collection** – A list of closely related basic products of a single type (e.g. observational data, browse files, documents, etc.). A collection is itself a product (because it is simply a list, with its label), but it is not a *basic* product.

**Data Object** – A generic term for an object that is described by a description object. Data objects include both digital and non-digital objects.

**Description Object** – An object that describes another object. As appropriate, it will have structural and descriptive components. In PDS4 a 'description object' is a digital object, such as a string of bits with a predefined structure.

Digital Object – An object which consists of electronically stored (digital) data.

**Identifier** – A unique character string by which a product, object, or other entity may be identified and located. Identifiers can be global, in which case they are unique across all of PDS (and its federation partners). A local identifier must be unique within a label.

**Label** – The aggregation of one or more description objects such that the aggregation describes a single PDS product. In the PDS4 implementation, labels are constructed using XML (eXtensible Markup Language).

**Logical Identifier** (LID) – An identifier that identifies the set of all versions of a product.

**Versioned Logical Identifier (LIDVID)** – The concatenation of a logical identifier with a version identifier, providing a unique identifier for each version of product.

**Metadata** – Data about data. For example, a 'description object' contains information (metadata) about an 'object.'

**Object** – A single instance of a class defined in the PDS Information Model.

**PDS Information Model** – The set of rules governing the structure and content of PDS metadata. While the Information Model (IM) has been implemented in XML for PDS4, the model itself is implementation independent.

**Product** – One or more labeled objects (digital, non-digital, or both) grouped together and having a single PDS-unique identifier. In the PDS4 implementation, if a product consists of multiple objects, their descriptions are combined into a single XML label. Although it may be possible to locate individual objects within PDS (and to find specific bit strings within digital objects), PDS4 defines 'products' to be the smallest granular unit of addressable data within its complete holdings.

**Registry** – A data base that provides services for sharing content and metadata.

**XML** schema – The definition of an XML document, specifying required and optional XML elements, their order, and parent-child relationships.

## 2. OVERVIEW

## 2.1 Purpose and Scope

The purpose of this Software Interface Specification (SIS) is to provide users of the InSight Deployment Arm (IDA) archive with a detailed description of the data products and how they are generated, along with a description of the PDS4 archive bundle, the structure in which the data products, documentation, and supporting material are stored. The users for whom this document is intended are software developers of the programs used in generating the higher data products, and scientists who will analyze the data, including those associated with the InSight mission and those in the general planetary science community.

This SIS covers data products generated by IDA and the higher level products derived from them that are intended to be archived in the Planetary Data System (PDS).

#### 2.2 Contents

This SIS describes how the IDA instrument acquires data, and how the data are processed, formatted, labeled, and uniquely identified. The document discusses standards used in generating the product and software that may be used to access the products. The data structure and organization are described in sufficient detail to enable a user understand the instrument, read the data and develop software to process these data.

## 2.3 Applicable Documents

- [1] Planetary Data System Standards Reference, version 1.11.0, October 1, 2018.
- [2] Data Provider's Handbook, Archiving Guide to the PDS4 Data Standards, version 1.11.0, October 1, 2018.
- [3] PDS4 Data Dictionary Document, Abridged, version 1.11.0.0, September 23, 2018.
- [4] PDS4 Information Model Specification, version 1.11.0.0, September 23, 2018.
- [5] InSight Archive Generation, Validation and Transfer Plan, JPL D-75289, May 30 2014.
- [6] InSight Flight-Ground Interface Document (FGICD), JPL D-75267.
- [7] Trebi-Ollennu, A., et al., InSight Mars Lander Robotics Instrument Deployment System (2018). Space Sci Rev, 214:93.
- [8] Soil mechanics IDA calibration Report (To be released after soil mechanics experiments have been performed)
- [9] Shaw, A., et al., Phoenix Soil Physical Properties Investigation (2009). J Geophys Res, 114
- [10] Smith, K., Technical Memorandum 20020233-B, Kinematic, Mass, and Stiffness Parameters of the Insight Robotic Arm
- [11] Collins, C.L. and Robinson, M.L., Accuracy Analysis and Validation of the Mars Science Laboratory (MSL) Robotic Arm, in Proceedings of the ASME 2013 International Design Engineering Technical Conferences and Computers and Information in Engineering Conference, Portland, Oregon, USA, 4-7 August 2013

- [12] Spong, M.W. and Vidyasagar, M., Robot Dynamics and Control (1989) John Wiley and Sons
- [13] Bonitz, R.G., et al., The Mars Surveyor '01 rover and robotic arm, in IEEE Aerospace Conference, Proceedings, vol. 7 (2000), pp. 235-246

The PDS4 Documents [1] through [4] are subject to revision. The most recent versions may be found at pds.nasa.gov/pds4. The IDA PDS4 products specified in this SIS have been designed based on the versions current at the time, which are those listed above. Data products will be static and will not be changed if new versions of documents [1] to [4] become available.

## 2.4 Audience

This document serves both as a Data Product SIS and an Archive SIS. It describes the format and content of IDA data products in detail, and the structure and content of the archive in which the data products, documentation, and supporting material are stored. This SIS is intended to be used both by the instrument team in generating the archive and by data users wishing to understand the format and content of the archive. Typically, these individuals would include scientists, data analysts, and software engineers.

## 2.5 InSight Mission

InSight was launched on May 5, 2018 and placed a single geophysical lander on Mars on November 26, 2018, to study its deep interior. The Surface Phase consists of Deployment and Penetration, and Science Monitoring. It ends after one Mars year plus 40 sols.

The science payload includes two instruments: the Seismic Experiment for Interior Structure (SEIS) and the Heat-Flow and Physical Properties Package (HP³). In addition, the Rotation and Interior Structure Experiment (RISE) uses the spacecraft X-band communication system to provide precise measurements of planetary rotation. SEIS and HP³ are placed on the surface with an Instrument Deployment System (IDS) comprising an Instrument Deployment Arm (IDA), Instrument Deployment Camera (IDC), and Instrument Context Camera (ICC). There are also several supporting instruments. The Auxiliary Payload Sensor Subsystem (APSS) includes the pressure sensor, the magnetometer, and Temperature and Wind for InSight (TWINS) sensors and collects environmental data in support of SEIS. These data are used by SEIS to reduce and analyze their data. The radiometer (RAD) is used by the HP³ team to measure surface temperature and thermal properties to support their data analysis. This document describes the IDA and the associated data products.

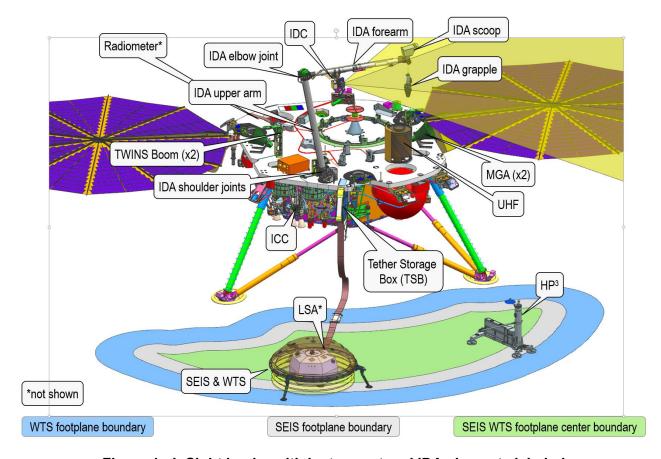


Figure 1 - InSight lander with instrument and IDA elements labeled

## 2.6 IDA Description

The purpose of the IDA is threefold: firstly, to deploy the SEIS, the SEIS Wind and Temperature shield (WTS), and HP<sup>3</sup> instruments from the InSight lander deck to the Martian surface; secondly, to point the IDC for imaging of the Martian terrain surrounding the InSight lander; thirdly, to perform soil mechanics experiments.

For more information about the IDA, refer to Trebi-Ollennu, et al. 2018 [7].

#### 2.6.1 IDA overview

The IDA is the flight Robotic Arm (RA) from the original Mars '01 lander. The various components of the IDA are illustrated in Figure 1 and Figure 2. The IDA is a four degree-of-freedom (DOF) back-hoe design manipulator that provides the following motion: yaw (shoulder azimuth, joint 1), and three pitch joints (shoulder elevation, elbow, and wrist, joints 2 through 4, respectively). Each of the IDA joints consists of a brushed DC motor with two-stage planetary gears and a harmonic drive at the output (except the wrist, which has a bevel gear at the output of the planetary gears). During normal operations, the IDA actuators are capable of generating 35, 120, 65, and 10.5 Newton-meters of torque at the joint output for joints 1 through 4, respectively. Each joint is equipped with a temperature sensor, a heater, and two position sensors: encoders on the joint input motor shaft and potentiometers at the joint output load shaft.

The IDA end-effector consists of a grapple, a scoop, and the IDC.

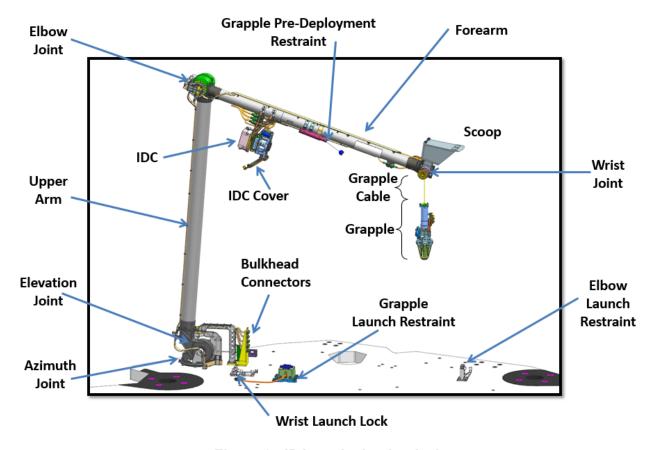


Figure 2 - IDA on the lander deck

#### 2.6.1.1 IDA End-Effectors

#### 2.6.1.1.1 IDA End-Effector Grapple

The grapple is a five finger "claw" and hangs by an umbilical cable at the IDA end-effector. Using the grapple, the IDA can lift and deploy a 9-kg payload on Mars (33N) at 1.65 m distance.

The grapple is stowed against the IDA forearm such that it does not obstruct the IDC Field of View (FOV). However, during deployment, the grapple is unstowed and hangs in the IDC FOV such

that the IDC images can capture the opening of the grapple fingers and engagement of spherical cap grapple hooks on the payload. The IDA can position the grapple to capture the payload's spherical cap grapple hook, lift, and place SEIS, WTS, and HP<sup>3</sup> on the Martian surface. The grapple can be re-stowed against the IDA after instrument deployment.

The grapple fingers are opened by a single High Input Paraffin (HOP) actuator that slowly heats up, melts the wax that pushes a rod out to open the fingers. As the grapple HOP cools down in the ambient temperature, the grapple fingers slowly close passively without any actuation.



Figure 3 - End-effector grapple with fingers closed (left) and fingers opened (right)

#### 2.6.1.1.2 IDA End-Effector Scoop

The scoop consists of a single chamber with a front blade and a secondary blade on the bottom side. The scoop will enable soil mechanics experiments for inferring mechanical properties of the Martian soil at the landing site. The scoop's applied force is configuration dependent, but the average force is typically about 80N. The scoop is not required for nominal instrument deployment operations.

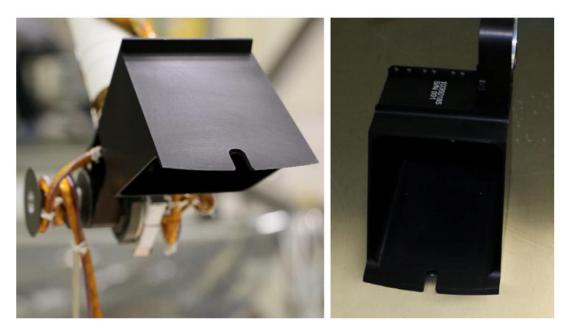


Figure 4 - End-effector scoop

#### 2.6.1.1.3 IDA End-Effector IDC

The IDC is a forearm mounted camera (closer to the elbow joint) facing the IDA end-effector. The IDA is used to point the IDC to take images of the surface, lander (selfie), lander elements, 360° panorama of the landing site, and other geological features at the landing site. The IDC allows visual confirmation of deployment steps, acquisition of the stereo image pairs used to create a 3D terrain map of the workspace, and provides engineering images of the solar arrays, payload deck, and instruments.



Figure 5 - End-effector IDC with dust cover opened

#### 2.6.1.2 IDA Motor Controller

The IDA Motor Controller (MC) consists of two printed-circuit boards located in the lower Payload Electronics Box (PEB) and provides power conditioning, motor voltage control and drivers, grapple heater drivers, joint encoder counting, and Analog-to-Digital (A/D) conversion of potentiometer voltages, temperature sensor voltages, motor currents, and heater current. The PEB provides the interface to the Lander Command and Data Handling (C&DH) computer via the InSight Payload Interface Card (IPIC) board. Firmware residing on the IDA MC microprocessor provides for low-level motor command execution to move the joints to the specified positions, grapple heater command execution, A/D calibration, and sensor monitoring.

#### 2.6.1.3 IDA Flight Software

The IDA Flight Software (FSW) provides both control of, and visibility into, the IDA hardware. It runs on board the C&DH computer and communicates with the PEB. IDA FSW provides to following specific capabilities:

- Interface with external entities, including other spacecraft FSW components and the IDA PEB
- Expansion of high-level IDA commands from the command sequencer into low-level IDA actions
- Motion control of the IDA
- Control of the grapple
- Fault sensing, recovery, and safing
- Collision prevention between the IDA, lander, and science instruments
- Visibility of the IDA state in telemetry

The IDA FSW responds to sequences of IDA commands which specify the desired movement in terms of the goal joint angles, a Cartesian position and approach angle for the specified tool, or a direction and length of time to move certain motors. IDA FSW breaks motion commands down into a sequence of via points describing intermediate joint positions to achieve the desired motion. The IDA FSW provides the command decomposition into via points, trajectory generation for each via point, and fault monitoring.

The IDA kinematics describe the geometrical relationships among the IDA elements. The forward kinematics maps IDA joint to the pose of the selected tool in Cartesian space. The inverse kinematics maps the pose of the tool to the corresponding joint angles. IDA FSW computes the forward and inverse kinematics to enable and determine IDA placement.

#### 2.6.2 IDA operations

#### 2.6.2.1 Workspace Imaging and Terrain Mosaic

Prior to deployment, an IDC stereo mosaic of the workspace is acquired to create a Digital Elevation Model (DEM) that provides information of the workspace terrain in 3-D coordinates. In order to minimize stereo baseline error, IDC stereo pairs are acquired by moving one IDA joint only – the shoulder joint (azimuth) – while keeping all the other joints constant. IDC workspace imaging is done in several tiers, starting with an inner tier close to the base of the lander and moving progressively outward. Only the IDA azimuth joint angle is changed within a tier. The IDA elbow joint angle is changed to move from one tier to the next. The IDC image data products are available online and are released via the PDS Cartography and Imaging Sciences Node (https://pds-imaging.jpl.nasa.gov/volumes/insight.html).

#### 2.6.2.2 Payload Deployment Steps

Each payload deployment (lift from the Lander deck to placement on surface) consists of four parts (Part 1, Part 2, Part 3, and Part 4).

- Part 1 of each payload deployment entails moving the unstowed grapple to the corresponding payload teach point. The payload teach points are 5 cm above the grapple hook position of the payload as stowed on the Lander deck.
- Part 2 consists of opening the grapple fingers and moving the fully open grapple fingers 4 cm down to capture the payload.
- Part 3 entails lifting the captured payload and placing it on the surface of Mars.
- Part 4 is called payload release, and it consists of opening the grapple and moving the IDA up and away from the payload grapple hook.

#### 2.6.2.3 Soil mechanics experiments

For the soil mechanics experiments, the IDA will be used as a science instrument to investigate the physical properties of the Martian surface at the InSight landing site. The IDA provides guarded motion capability, a single command that allows the IDA to be commanded to move to a position until contact is made. Guarded move command capability will enable the IDA soil mechanics experiments, that consist of indentation tests. Analysis that used similar data products to infer soil physical properties from the Robotic Arm activities during the Phoenix mission can be found in [9].

#### 2.6.3 IDA calibration

On the ground, two thermal characterization tests were performed on the IDS subsystem in a thirteen-foot Sensor Chamber at the Raytheon El Segundo Integrated Test Laboratory (ITL), California. During the test, the IDA heaters were characterized and IDA functional qualification was successfully performed at proto-flight operational temperature. In addition, IDA stop-and-hold torques were characterized at various temperatures.

## 3. IDA DATA PRODUCTS

#### 3.1 Data Product Overview

IDA data products consist of raw observations and calibrated data. When the IDA is commanded and operational, Science/Engineering Low Priority (SciLo) and Science/Engineering High Priority (SciHi) data products are provided. Additionally, IDA status, IDA history, and IDA parameters are downlinked and included in this archive. Supplemental RSVP Replay Videos generated using the Rover Sequencing and Visualization Program (RSVP) are included in the PDS archive when the soil mechanics experiments are performed.

Table 4 shows a summary of IDA data products. See Table 5 for processing level definitions. Details about each product can be found in Section 5.

| Product  | <b>Processing level</b> | Storage format    |
|--|-------------------------|-------------------|
| IDA status                                     | Ancillary               | ASCII table       |
| IDA history                                    | Ancillary               | ASCII table       |
| IDA parameters                                 | Ancillary               | ASCII table       |
| Science/Engineering Low Priority (SciLo) data  | Raw/Calibrated          | ASCII text tables |
| Science/Engineering High Priority (SciHi) data | Raw/Calibrated          | ASCII text tables |

Table 4 - IDA data products overview

## 3.2 Data Processing

This section describes the processing of IDA data products, their structure, organization, and labeling.

## 3.2.1 Data Processing Level

Data processing levels mentioned in this SIS refer to the PDS4 processing level described in Table 5. The lowest processing level archived in PDS is "raw" as described in the table. PDS does not archive telemetry.

PDS4 processing level PDS4 processing level description

Original data from an experiment. If compression, reformatting, packetization, or other translation has been applied to facilitate data transmission or storage, those processes are reversed so that the archived data are in a PDS approved archive format. Often called EDRs (Experimental Data Records).

Partially Processed

Data that have been processed beyond the raw stage but which have not yet reached calibrated status. These and more highly processed products are often called RDRs (Reduced Data Records).

Data converted to physical units, which makes values independent

Results that have been distilled from one or more calibrated data

products (for example, maps, gravity or magnetic fields, or ring particle size distributions). Supplementary data, such as calibration tables or tables of viewing geometry, used to interpret observational data should also be classified as 'derived' data if not easily matched

**Table 5 - Data Processing Level Definitions** 

IDA data product described in this SIS are a hybrid of raw and calibrated processing levels.

of the experiment.

#### 3.2.2 Data Product Generation

Calibrated

Derived

When the IDA is commanded and operational, it generates blocks of data in regular intervals which are stored on-board. Upon further commanding, the stored data is processed on-board by the downlink processor and sent down to Earth in telemetry packets. See Appendix C for the structure of the IDA primary data format.

to one of the other three categories.

On the ground, the Multimission Instrument Processing Laboratory (MIPL) subsystem is responsible for processing these packets and generating instrument products which are collections of time based, sorted packets. The IDA generates and downlinks a number of different data types, known as Application Identifier (APID). Data for each APID is stored as a separate product. Packets with different APIDs contain different type of data, with different structure.

The MIPL subsystem collects and processes six different telemetry data for the IDA. They are listed in Table 6.

Table 6 - IDA telemetry data processed by MIPL

| APID | Description        |
|------|--------------------|
| 84   | Collision database |

| 85 | IDA history, from onboard ring buffer of 300 status products (APID 89) |
|----|--|
| 86 | IDA internal parameters and configuration                              |
| 87 | Science/Engineering data, high downlink priority                       |
| 88 | Science/Engineering data, low downlink priority                        |
| 89 | IDA status   |

MIPL generates four types of data products for IDA:

- Collision data product for APID 84
- History and status products for APIDs 85 and 89
- Parameter and configuration for APID 86
- Science and engineering for APIDs 87 and 88

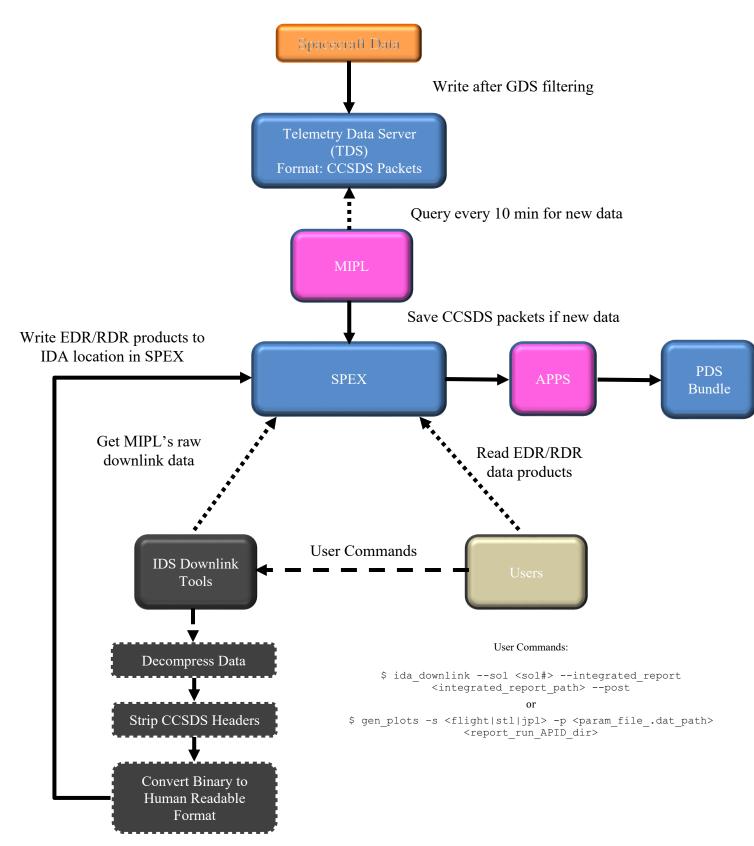
The format and structure for all the products is similar. The files contain the original CCSDS (Consultative Committee for Space Data Systems) packets for a given APID from a given downlink, DSN pass. It is possible to have a gap, or a jump, in the SCLK, but the packets will always be sorted by SLCK. If there are packets that are missing for a given downlink, they will be put into the file/product that is generated for the future pass that contains that data.

#### 3.2.3 Data Flow

This section describes only those portions of the InSight data flow that are directly connected to IDA archiving. A full description of InSight data flow is provided in the InSight Archive Generation, Validation, and Transfer Plan [5].

IDA data are downlinked by InSight Project Operations at JPL. The JPL Advanced Multimission Operations System (AMMOS) Multimission Instrument Processing Laboratory (MIPL) delivers raw CCSDS telemetry packets to the IDA team at JPL. The IDA team extracts raw data products from the packets. The MIPL team generates PDS4 labels for all the IDA data products, assembles the data and documentation into IDA archive bundles, and delivers the bundles to the PDS Geosciences Node. Deliveries take place according to the release schedule agreed upon by the InSight Project and PDS and specified in the InSight Archive Plan. The Geosciences Node validates the bundles for PDS4 compliance and for compliance with this SIS document, and makes them available to the public online.

## Spacecraft IDA Data Flowchart



## 3.3 Standards Used in Generating Data Products

The IDS data products comply with the Planetary Data System PDS4 standard for science data archives, as specified in the PDS Standards Reference [1], the Planetary Science Data Dictionary Document [3], and the PDS4 Information Model Specification [4]. These standards documents are revised approximately every six months. The version that is current at the time of the IDA peer review is used for the archive. See Section 4, for a description of the PDS Label and the specific conventions.

#### 3.3.1 Time Standards

PDS labels for InSight data products allow the use of various time-related attributes. The following are used in labels for IDA products.

| Time value                          | Label attribute*   | Formation rule  |
|-------------------------------------|--|---|
| UTC time of observation             | start_date_time,<br>stop_date_time   | yyyymmddThh:mm:ss.ffffffZ   |
| Sol (Mars day) of observation       | sol_number, or the pair<br>start_sol_number,<br>stop_sol_number                                      | A non-negative integer (landing day is Sol 0)   |
| Spacecraft clock count (SCLK)       | spacecraft_clock_start count,<br>spacecraft_clock_stop_count   | [p/]dddddddddd[-fffff] where p = partition number, ddddddddddd = whole seconds, fffff = fractional seconds as 1/65536 ticks |
|                                     | spacecraft_clock_count_partition<br>must be used if SCLK values do not<br>include a partition number | A positive integer  |
| *Attributes start_date_time and sto | p_date_time are defined in the PDS4 core   | dictionary. The others are defined in   |

the InSight Mission Dictionary.

See an example of IDA label in Appendix E.

## 3.3.2 Coordinate Systems

This section describes the primary coordinate systems defined for surface operations, which are listed in Table 7 and illustrated in Figure 6 below.

**Table 7 - Coordinate Frames Used for Surface Operations** 

| Name                                | Label Keyword       | Origin   | Orientation  |
|-------------------------------------|---------------------|--|--|
| Payload Frame (P Frame) (IDA Frame) | "PAYLOAD_F<br>RAME" | Attached to Lander at intersection of IDA joint 1 rotation axis and the top surface of the lander deck | Fixed offset frame rotated 180 deg about +Z axis relative to Lander frame:  • +Z axis is normal to deck surface and points from that surface downward. |

|   |                             |   | <ul> <li>+X axis is perpendicular to Z axis and points towards IDA side of deck.</li> <li>+Y completes the right-handed frame.</li> </ul>   |
|---|-----------------------------|---|---|
| Lander Frame (L Frame) NOTE: Not used in Surface Operations | does not appear<br>in label | Centered on launch vehicle separation plane 956.056 mm above Lander deck. Lander Mechanical frame origin relative to the Payload Frame = [-775.084, -283.360, -956.056] | <ul> <li>Aligned with Lander:</li> <li>+Z axis is normal to deck surface and points from that surface downward.</li> <li>+X axis is perpendicular to Z axis, parallel to solar array yoke and points toward deck side opposite to IDA.</li> <li>+Y completes the right-handed frame.</li> </ul> |
| IDC Frame (S <sub>IDC</sub> Frame)                          | does not appear in label    | Attached to Camera  | Aligned with camera pointing  |
| Site (S <sub>N</sub> Frame) (Surface Frame)                 | does not appear<br>in label | Attached to Surface   | Aligned with Lander:  • +Z axis points downward to Nadir (gravity vector).  • +X axis is perpendicular to Z axis and points towards North.  • +Y completes the right-handed frame and points East.  |
| Local Level (L <sub>L</sub> Frame)                          | does not appear<br>in label | Attached to Lander<br>(coincident with<br>Payload Frame)  | Fixed offset frame relative to Site frame:  • +Z axis points downward to Nadir (gravity vector).  • +X axis is perpendicular to Z axis and points towards North.  • +Y completes the right-handed frame and points East.  |
| SEIS ASM (Frame)  |                             | Centered at SEIS grapple hook   | The main frame used by the SEIS team. It is fixed to SEIS:  • +Z axis is upwards  • +X axis is oriented from the sphere center to the dampers located at 36 degrees of the sphere valve  • +Y axis completes the right-handed coordinate frame  |
| SEIS Grapple Hook<br>Frame                                  |                             | Centered at SEIS grapple hook   | Defined along the tether:  • +Z axis is co-aligned with the IDA Z axis and is also fixed to SEIS  |

|  | +X axis is along the tether on<br>the deck and fixed to SEIS so<br>the X axis always faces the<br>opposite direction of the LSA |
|--|---|
|  | • +Y axis completes the right-handed coordinate frame   |

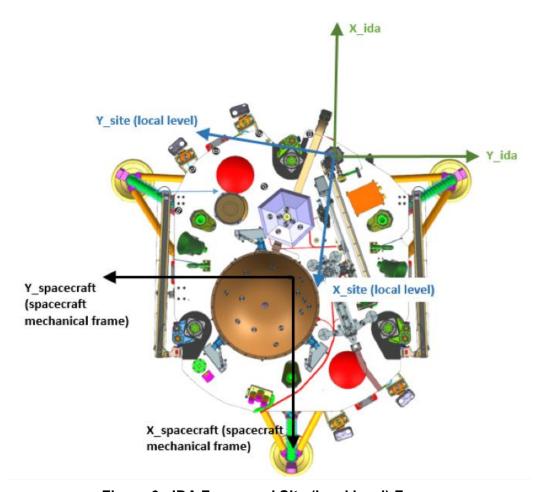


Figure 6 - IDA Frame and Site (local level) Frame

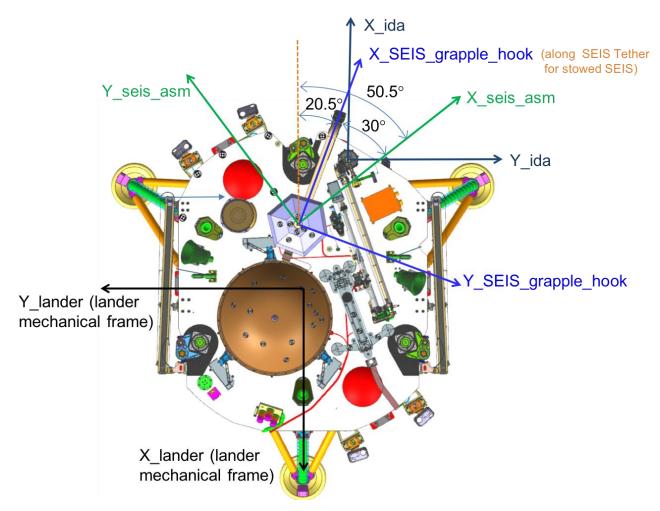


Figure 7 - IDA, SEIS ASM, and SEIS Grapple Hook Coordinate Frames

## 3.3.3 Data Storage Conventions

IDA products are stored as ASCII fixed-width tables.

## 3.4 Applicable Software

IDA data in ASCII tables may be read using many text editors and spreadsheet programs. No special software is required for use with IDA data.

## 3.5 Backups and Duplicates

The Geosciences Node keeps online copies of each archive product. One copy is the primary online archive copy. Another is a backup copy. Once the archive products are fully validated and approved for inclusion in the archive, another copy of the archive is sent to the National Space Science Data Center (NSSDC) for long-term preservation in a NASA-approved deep-storage facility. The Geosciences Node may maintain additional copies of the archive products, either onor off-site as deemed necessary according to the Node's backup and disaster recovery plan.

## 4. IDA ARCHIVE ORGANIZATION, IDENTIFIERS AND NAMING CONVENTIONS

This section describes the basic organization of the IDA data archive under the PDS4 Information Model (IM) (Applicable documents [1] and [3]), including the naming conventions used for the bundle, collection, and product unique identifiers. The formation of logical identifiers is described in Section 4.1. Bundles, collections and products are defined and given identifiers in Section 4.2. In short, a group of related products forms a collection, and a group of related collections forms a bundle.

## 4.1 Logical Identifiers

Every product in PDS is assigned a Logical Identifier (LID) that allows it to be uniquely identified across the system. Each product also has a Version Identifier (VID) that allows different versions of a specific product to be referenced uniquely. A product's LID and VID are defined as separate attributes in the product label. For convenience they may be combined in a single string called a LIDVID, with two colons between the LID and the VID. If a particular version of a product is desired, the LIDVID should be used; otherwise the LID alone should be used with the understanding that it refers to the latest version of the product.

LIDs and VIDs are assigned by PDS and are formed according to the conventions described in the following sections. More information on LIDs and VIDs may be found in Section 6d of the PDS Standards Reference [1] and in Chapter 5 of the Data Providers' Handbook [2].

#### 4.1.1 LID Formation

LIDs take the form of a Uniform Resource Name (URN). LIDs are restricted to ASCII lower case letters, digits, dash, underscore, and period. Colons are also used, but only to separate prescribed components of the LID. Within one of these prescribed components dash, underscore, or period are used as separators. LIDs are limited in length to 255 characters.

InSight IDA LIDs are formed according to the following conventions:

• Bundle LIDs are formed by appending a bundle-specific ID to the PDS base ID:

urn:nasa:pds:<bundle ID>

Example: urn:nasa:pds:insight ida

The bundle ID must be unique across all bundles archived with the PDS.

• Collection LIDs are formed by appending a collection-specific ID to the collection's parent bundle LID:

urn:nasa:pds:<bundle ID>:<collection ID>

Example: urn:nasa:pds:insight ida:data ancillary

The collection ID must be unique across the bundle. Collection IDs correspond to the collection type (e.g. "browse", "data", "document", etc.). Additional descriptive information may be appended to the collection type (e.g. "data-raw", "data-calibrated", etc.) to ensure that multiple collections of the same type within a single bundle have unique LIDs.

• Basic product LIDs are formed by appending a product-specific ID to the product's collection LID:

urn:nasa:pds:<bur>dle ID>:<collection ID>:product ID>

Example:urn:nasa:pds:insight\_ida:data\_ancillary:a0089\_0062\_602047157\_60205 2923 190129195008 006 arm float

The product ID must be unique across the collection. For IDA data products, the product LID is the same as the lower case data file name without the extension.

#### 4.1.2 VID Formation

Product Version IDs consist of major and minor components separated by a "." (M.n). Both components of the VID are integer values. The major component is initialized to a value of "1", and the minor component is initialized to a value of "0". The minor component resets to "0" when the major component is incremented. The PDS Standards Reference [1] rules for incrementing major and minor components.

## 4.1.3 File Naming Conventions

All IDA data products are named according to the following naming conventions:

| Α | APID | - | Start Sol | Start Sclk | - | End Sclk  | - | уу | mm | dd | hh | mm | SS | - | Product Identifier |
|---|------|---|-----------|------------|---|-----------|---|----|----|----|----|----|----|---|--------------------|
| A | 0089 | 1 | 0062      | 602047157  | 1 | 602052923 | 1 | 19 | 01 | 29 | 19 | 50 | 08 | ı | 006_arm_float.txt  |

#### Where:

- A indicates that the product is an IDA product
- [APID] identifier specifies the APID number (Table 6) as a four digit number
- [Start Sol] identifier specifies the Martian sol (counted after InSight landing) when the data started to be collected by the instrument as a four digit number
- [Start SCLK] identifier specifies the SCLK of the earliest packet as a nine digit number
- [End SCLK] identifier specifies the SCLK of the latest packet as a nine digit number
- [yy][mm][dd][hh][mm][ss] is the time tag identifier and corresponds, respectively, to the numerical value of year, month, day, hours, minutes and seconds UTC when the data started to be collected by the IDA
- [Product] identifier specifies the data product and its file extension. It can be one of the following:

 Data Product
 [Product] identifier

 IDA status
 006\_arm\_float.txt

 IDA history
 000\_system\_float.txt

 IDA parameters
 012.txt

 Engineering/Science Low Priority (SciLo)
 eu.csv

 Engineering/Science High Priority (SciHi)
 eu.csv

**Table 8 - File Naming Convention** 

An example of data product name is:

A0089 0062 602047157 602052923 190129195008 006 arm float.txt

This file contains IDA status data collected starting on sol 62 of the mission, with a starting SCLK time of 602047157 and an end SCLK time of 602052923, starting data acquisition on the 29<sup>th</sup> of January 2019 at 19:50:08 UTC.

#### 4.2 IDA Bundles

The highest level of organization for a PDS archive is the bundle. A bundle is a set of one or more related collections which may be of different types. A collection is a set of one or more related basic products which are all of the same type. Bundles and collections are logical structures, not necessarily tied to any physical directory structure or organization.

The complete InSight IDA archive is organized into one bundle (Table 9).

 Bundle Logical Identifier
 PDS4 Processing Level
 Description

 urn:nasa:pds:insight\_ida
 The insight\_ida bundle contains collections for IDA raw data, and documentation, including time-lapse videos of data acquisition.

Table 9 - IDA Bundle

In addition to the IDA data bundle, the InSight archives have a Document Bundle that contains documentation for all InSight data bundles, including IDA documents. The contents of the Document Bundle are described in Section 4.5.

## 4.3 IDA Collections

The IDA Bundle contains the collections listed in Table 10.

Table 10 - Collections in the IDA Bundle

| Collection Logical Identifier                | Collection<br>Type | Description   |
|--|--------------------|---|
| urn:nasa:pds:insight_ida:data_ancillary      | Ancillary data     | IDA status, history, and parameters   |
| urn:nasa:pds:insight_ida:data_raw_calibrated | Data               | Hybrid raw and calibrated IDA data products   |
| urn:nasa:pds:insight_ida:document_video      | Document           | Time-lapse videos of data acquisition   |
| urn:nasa:pds:insight_documents:document_ida  | Document           | Documentation, including the Software Interface Specification (SIS) and the Soil mechanics calibration report |

## 4.4 IDA Products

An IDA science data product consists of one digital object in one file, accompanied by a PDS label file. The PDS label provides identification and description information for the data file. As discussed above, the PDS label includes a Logical Identifier (LID) by which the product is uniquely identified throughout all PDS archives. Under the PDS4 standard, labels are XML-formatted ASCII files.

In addition to data products, the IDA archive contains document products. These also have PDS labels.

Finally, the collections and bundles themselves are considered "products" in PDS, and have their own PDS labels.

## 4.5 InSight Document Bundle and Collections

Documents are also considered products in PDS, and have LIDs, VIDs and PDS4 labels just as data products do. The InSight archives include an InSight Document Bundle, which consists of collections of documents relevant to the mission itself and all the science experiments. The IDA Team is responsible for the IDA document collection in this bundle.

**Table 11 - Collections in the InSight Document Bundle** 

| Collection Logical Identifier                   | Description  |
|---|--|
| urn:nasa:pds:insight_documents:document_mission | InSight mission, spacecraft and lander descriptions                            |
| urn:nasa:pds:insight_documents:document_apss    | APSS SIS, instrument description, and other relevant documents                 |
| urn:nasa:pds:insight_documents:document_camera  | Camera SIS, instrument description, and other relevant documents               |
| urn:nasa:pds:insight_documents:document_hp3rad  | HP <sup>3</sup> /RAD SIS, instrument description, and other relevant documents |
| urn:nasa:pds:insight_documents:document_ida     | IDA SIS (this document), instrument description, and other relevant documents  |
| urn:nasa:pds:insight_documents:document_mag     | MAG SIS, instrument description, and other relevant documents                  |
| urn:nasa:pds:insight_documents:document_rise    | RISE SIS, instrument description, and other relevant documents                 |
| urn:nasa:pds:insight_documents:document_seis    | SEIS SIS, instrument description, and other relevant documents                 |
| urn:nasa:pds:insight_documents:document_spice   | SPICE relevant documents   |

In PDS4 a collection may belong to more than one bundle. It is a primary member of one bundle – the one on which its LID is based – and a secondary member of other bundles. The collection **urn:nasa:pds:insight\_documents:document\_ida** is a primary member of the InSight Document

Bundle and a secondary member of the IDA Bundle. The actual files that comprise the collection are found in the bundle where it is a primary member. They do not have to be duplicated in the other bundles, although they may be.

## 5. IDA ARCHIVE PRODUCT FORMATS

Data that compose the IDA data archive are formatted in accordance with PDS specifications (Applicable Documents [1], [2], and [3]). This section provides details on the formats used for each of the products included in the archive.

### 5.1 Data Product Formats

This section describes the format and record structure of each of the data file types. IDA data products will be stored as ASCII text tables and ancillary ASCII files.

#### 5.1.1 IDA Status

IDA arm status files contain reported values from the PEB. The status data is the following:

```
ra status.ace.calib OK
ra status.ace.bus30v err = 0
ra status.ace.parity err = 0
ra status.ace.msg err
                        = 0
ra status.ace.load box
ra status.ace.self test
ra status.mtr.pwr on
                       0 ] =
                                0
                                    0
                                        0 ]
ra status.mtr.rotation
                      0 ] =
                               0
                                    1
ra_status.mtr.over_current = [ 0
                                 0
                                      0
                                           0 ]
ra status.mtr.brake
                      = [ 0
                               0
                                  0
                      = [ 0.000 0.001 0.000 0.001]
ra status.mtr.current
                     = [-0.100 -0.320 1.010 0.134 ]
ra status.jnt.enc
ra status.jnt.pot
                    = [-0.100 -0.321 1.009 0.134 ]
ra_status.jnt.temp
                     = [ 26.512 26.656 28.098 28.538 ]
                   = [ 4.502 -4.498 ]
ra status.ref
ra_status.htr crnt
                     = 0.001
ra status.agnd
                     = 0.002
ra status.time
                    = 594733695.9
```

- ra status.ace.calib OK Boolean whether PEB calibration is nominal.
- ra status.ace.bus30v err Boolean whether PEB 30v Bus is in an error state.
- ra status.ace.parity err Boolean whether PEB parity bit is in an incorrect state.
- ra status.ace.msg err Boolean whether PEB command had format error.
- ra\_status.ace.load\_box Boolean whether PEB load box is present. Note that this value should always be 0 for flight.
- ra status.ace.self test Boolean whether PEB is in a self-test state.
- ra status.mtr.power on joint 1, joint 2, joint 3, joint 4 boolean if motor is on.
- ra status.mtr.rotation joint 1, joint 2, joint 3, joint 4 direction of rotation.
  - $\circ$  0 positive
  - $\circ$  1 negative

- ra\_status.mtr.over\_current joint 1, joint 2, joint 3, joint 4 boolean whether an over-current has been detected.
- ra\_status.mtr.brake joint 1, joint 2, joint 3, joint 4 boolean whether motor brake is on
   0 off
   1 on
- ra\_status.mtr.current joint 1, joint 2, joint 3, joint 4 current in amps
- ra\_status.ref vref1, vref2 reference voltage in volts
- ra status.htr crnt Sum of heater currents in amps
- ra status.agnd Analog ground value in volts
- ra status.time The last time (SCLK) when the above data was acquired from the PEB

IDA system status files contain reported values from IDA FSW. During a motion command, the status values are recorded at a constant rate. During a non-motion command, the status values are recorded if there is a change from the last recorded values. The status data is the following:

```
= [ 172 325 273 190 ]
sys status.curr limit
sys status.mtr volt
                           =[2121]
sys status.brake
                           = [0000]
sys status.use pots
                            =[00001
sys status.htr on
                           = [00001]
                          = 5 RA GRAPPLE
sys status.tool
sys status.cool down
                             = 0
sys status.fault chk mask
                               = [F00F0F 39FF7E7F]
svs status.fault status
                            [00]
                            = 23 RA SEND DATA
sys status.act cmd
sys status.act args
                            = 220
                             = 23 RA_SEND_DATA
sys status.task cmd
sys status.task args
                            = 220
                           = [ 0.026 -0.389 1.378 0.125 ]
sys status.target.g
                           = [ 0.960 0.218 -0.098 0.992 ]
sys status.target.x
sys status.via.q
                          = [-0.829 -1.640 0.230 0.000]
sys status.via.x
                          = [ 0.210 0.036 -1.580 1.501 ]
sys status.via step
sys status.via time
                            = 602049408.2
sys status.col status.has collisions = 0
sys status.col status.link1
                              = -1
sys status.col status.link2
                              = -1
sys status.col status.obj1
                              = -1
sys status.col status.obj2
                              = -1
sys status.rotation cmd
                              =[1-111]
                             = [ 0.000 0.000 0.000 0.000 ]
sys status.delta via.dq
sys status.delta via.dx
                             = [ 0.000 0.000 0.000 0.000 ]
sys status.delta via.mag
                              = 0.0000
sys status.algo code
                             = 2 RA ALGO CONTACT
                                 = 0 RA ALGO NO OVERRIDE
sys status.algo code override
sys status.delta via code
                               = 3 RA DELTA VIA USER
sys status.plane angle
                              = 0.0097
sys status.tau
                          = [ 0.0 0.0 0.0 0.0 ]
sys status.delta tau
                            = 0.0000
                             = 0 RA NO TRACKING
sys status.track state
sys status.energy limit
                             = 0.0
sys status.energy value
                              = 0.0
```

```
sys_status.time_limit = 602049206.7
sys_status.grapple_state = 0 Fingers-Open
sys_status.grapple_temp = 99.5
sys_status.grapple_exp_time = 0.000000
sys_status.grapple_phase = 2 RA_OK_TO_OPEN
sys_status.mtr_volt_sign = [ 0 0 0 0 ]
sys_status.actively_holding_position = 0
sys_status.time = 602050014.0
```

- sys status.curr limit Joint current limits (mA)
- sys status.mtr volt Joint motor voltages (V)
- sys\_status.brake Boolean for whether the brakes are applied on each joint when the command is complete
- sys\_status.use\_pots Boolean for whether to use the pots on each joint for motion control
- sys\_status.htr\_on Boolean for whether the heater is on for each joint
- sys\_status.tool Selected tool (blade 1 | blade 2 | IDC | scoop | wrist | grapple | grapple-attach)
- sys status.cool down Boolean for whether cool down activity is active
- sys\_status.fault\_chk\_mask Fault mask code that is enabled for joint and misc. The value will be 0 if all faults are disabled
- sys\_status.fault\_status Fault mask code for which faults have tripped for joint and misc. The value will be 0 if there are no faults
- sys status.act cmd Last actuator command
- sys status.act args Arguments for last actuator command
- sys status.task cmd Last non-actuator command
- sys status.task args Arguments for last non-actuator command
- sys status.target.q Target joint position in radians of the last RA MOVE GUARDED
- sys\_status.target.x Target Cartesian position and orientation of the last RA MOVE GUARDED
- sys status.via.q Joint position in radians of the current via point
- sys status.via.x Cartesian position and orientation of IDA
- sys status.via step The via point that the IDA is moving towards
- sys status.via time During a timed joint move, the time (sclkd) that the current via point started
- sys status.col status.has collisions Boolean for existence of collision
- sys status.col status.link1 linkID of the RA link having collisions or -1 if none
- sys status.col status.link2 linkID of the other link
- sys status.col status.obj1 object ID of one object
- sys\_status.col\_status.obj2 object ID of the other object
- sys\_status.rotation\_cmd Two possible values to represent direction, -1 for negative direction and 1 for positive direction. If the IDA is moving, the value is current direction. If the IDA is not moving, the value is the last recorded direction.
- sys status.delta via.dq Modification of joint position in radians based on dx
- sys\_status.delta\_via.dx Modification of Cartesian position and orientation based on torque monitoring during accommodation
- sys status.delta via.mag Magnitude of delta via
- sys\_status.algo\_code Torque threshold (1=accomodate, 2=contact, 3=free space)
- sys\_status.algo\_code\_override Override or not override the torque threshold. If not set to override, then use algo code; otherwise, use this algo code override value
- sys\_status.delta\_via\_code Index (0=acq,1=dig,2=scrape,3=user) into parameter to determine direction of accommodation to limit elevated joint torques

- sys\_status.plane\_angle When using a scrape command, angle (radians) of scrape relative to the x-y plane
- sys status.tau Joint torques (N-m)
- sys\_status.delta\_tau Updated torque (N-m) from delta via computation, normalized value of the joint torque above its threshold
- sys\_status.track\_state State of resource tracking: {RA\_NO\_TRACKING=0, RA\_TRACK\_ENERGY=1, RA\_TRACK\_TIME=2, RA\_TRACK\_BOTH=3}
- sys\_status.energy\_limit If sys\_status.track\_statue is RA\_TRACK\_ENERGY, value is amount of energy (Watt-hours) not to exceed
- sys\_status.energy\_value If sys\_status.track\_statue is RA\_TRACK\_ENERGY, value is amount of energy (Watt-hours) used
- sys\_status.time\_limit If sys\_status.track\_statue is RA\_TRACK\_TIME, value is limit in minutes for the current command
- sys\_status.grapple\_state Grapple state (0=in-between, 1=closed, 2=open, 3=broken) based on the four combinations of the limit switch states
- sys\_status.grapple\_temp Grapple temperature (C)
- sys status.grapple exp time Time (sclkd) that the grapple stops heating
- sys\_status.grapple\_phase Grapple phase (launch\_locked | stowed | ok\_to\_open | seis grappled | wts grappled | hp3 grappled)
- sys\_status.mtr\_volt\_sign Motor voltage sign (1 is positive and -1 is negative) during active hold, 0 otherwise
- sys status.actively holding position Boolean for whether active hold is active
- sys\_status.time Time (sclkd) the system status values were recorded

## 5.1.2 IDA History

The history file contains the chronological concatenation of the last 300 status outputs (both arm and system) from the point when the dump history command is initialized. Details regarding IDA status can be found in Section 5.1.1.

In the history file, the point value goes in descending order starting at 299 and ends at 0. Also provided is the index value of the heap that stores the state and history data. Note that the heap size is 300 and the values will be overwritten once the heap is full. The point and index value are shown in the IDA history file as:

0 points before latest (index = 295):

#### 5.1.3 IDA Parameters

The parameter file contains a timestamp (SCLK) and the following parameters:

## 5.1.3.1 RA\_ARM\_PARAMS

```
Parameter Set: RA_ARM_PARAMS
dh.a = [ 0.029609000  0.976664007  0.857989013  0.0000000000  ]
dh.d = [ -0.056456000 -0.140837997  0.0000000000  0.000000000  ]
dh.alpha = [ 1.570799947  0.0000000000  0.0000000000  1.570799947  ]
x_blade_1 = [ -0.015010000  0.0000000000  0.105240002  0.000000000  ]
x_blade_2 = [ -0.015010000  0.0000000000  0.105240002  0.000000000  ]
x_rac = [ -0.560000002 -0.055000000 -0.150000006  1.570799947  ]
```

- dh.a joint1, joint2, joint3, joint4 Denavit and Hartenberg (DH)<sup>1</sup> link lengths (m).
- dh.d joint1, joint2, joint3, joint4 Denavit and Hartenberg (DH))<sup>1</sup> link offsets (m).
- dh.alpha joint1, joint2, joint3, joint4 Denavit and Hartenberg (DH))<sup>1</sup> frame twists (rad).
- $x_blade_1 x$ , y, z, theta coordinates of the forward-facing scraping blade in the wrist frame (x, y, z in m and theta in rad).
- x\_blade\_2 x, y, z, theta coordinates of the backward-facing scraping blade in the wrist frame (x, y, z in m and theta in rad).
- x rac x, y, z, theta coordinates of the IDC in the wrist frame (x, y, z in m) and theta in rad).
- x\_scoop x, y, z, theta coordinates of the scoop blade in the wrist frame (x, y, z in m and theta in rad).
- x wrist x, y, z, theta coordinates of the wrist in the wrist frame (x, y, z in m) and theta in rad).
- x\_grapple\_attach x, y, z, theta coordinates of the grapple-attach frame in the wrist frame (x, y, z in m and theta in rad).
- dist\_grapple Element 2 (third element) is the distance between the Grapple-Attach frame and the Grapple frame (m). The other elements must be zero.
- dist\_seis Element 2 (third element) is the distance between the Grapple-Attach frame and the SEIS frame (m). The other elements must be zero.
- dist\_wts Element 2 (third element) is the distance between the Grapple-Attach frame and the WTS frame (m). The other elements must be zero.
- dist\_hp3 Element 2 (third element) is the distance between the Grapple-Attach frame and the HP3 frame (m). The other elements must be zero.

## 5.1.3.2 RA\_JOINT\_PARAMS

```
Parameter Set: RA JOINT PARAMS
q min
            = [-3.5314
                          -2.3953
                                     -0.4324
                                               -0.1742
             = [ 1.4585
                                               3.5887
q max
                           1.307
                                     4.0478
                                                         ]
pot.b
           = [ 1394.31
                           2175.06
                                     955.99
                                                1491.77
pot.m
                           685.114
                                      691.49
                                                681.93
            = [-683.776]
            = [ 2048
                          2048
                                    2048
                                              2048
current.b
             = [ 0.00032143  0.00032143  0.00032143  0.00032143  ]
current.m
                         2048
vref.b
           = [ 2048
vref.m
            = [ 0.00225
                           0.00225
             = [ -12500
                                      10000
                                                4000
gear ratio
                           16000
                                                  3.1416
               = [ 3.1416
                             3.1416
                                       3.1416
rad per enc
             = [-0.544255018 0.824948013 0.237636998 0.305449992]
enc offset
htr power
             = [ 14.1
                           3.1
                                   11.2
                                             11.2
                         3
start count
             = [5
                                 3
                                          3
                                                 ]
                           1
                                   1
                                           1
nonstart count. = [ 1
                          85
                                   85
                                            85
direction crnt = [ 85
```

<sup>&</sup>lt;sup>1</sup> See Appendix B for definition of Denavit and Hartenberg link frames

| direction delay =   50 50 50 50 |
|---------------------------------|
|---------------------------------|

- q min joint1, joint2, joint3, joint4 minimum joint angles (rad).
- q\_max joint1, joint2, joint3, joint4 maximum joint angles (rad).
- pot.b joint1, joint2, joint3, joint4 pot offset (LSBs). Digital number values that the PEB reports when the engineering unit value is 0 for the joint angle measured by the potentiometer.
- pot.m joint1, joint2, joint3, joint4 pot slope (LSB/rad).
- current.b joint1, joint2, joint3, joint4 motor current offset (LSBs). Current reference value when the joint angle is zero.
- current.m joint1, joint2, joint3, joint4 motor current slope (amps/LSB).
- vref.b vref1, vref2 voltage reference offset (LSBs). Voltage reference value when the joint angle is zero.
- vref.m vref1, vref2 heater2 voltage reference slope (volts/LSB).
- gear ratio joint1, joint2, joint3, joint4 gear ratios
- rad\_per\_enc joint1, joint2, joint3, joint4 radians per encoder pulse at the motor shaft. To convert to joint angle, divide by the *gear\_ratio*.
- enc\_offset joint1, joint2, joint3, joint4 encoder offset (LSBs). This value was chosen such that when the encoder count is 1000 (this prevents rollover), the computed joint angle equals q\_min. Also, even though the encoder is physically located on the motor shaft, enc\_offset is expressed as if it were on the joint output. I.e., multiply by the gear\_ratio to convert to the equivalent value at the motor shaft.
- htr power joint 1, 2, and 3, joint 4, grapple heater 1, grapple heater 2 heater power (watts)
- start\_count joint1, joint2, joint3, joint4 the number of current samples the firmware ignores immediately after the motor is powered on. During this time zero current will be reported in the response. A value of FF will disable overcurrent monitoring and will cause zero current to be reported in the response, *always*.
- nonstart\_count joint1, joint2, joint3, joint4 the number of consecutive overcurrent samples the firmware ignores at any time after the startup count. A value of FF will disable overcurrent monitoring.
- direction\_crnt joint1, joint2, joint3, joint4 current (mA) above which the encoder count direction is reversed when the motor is stopped. Below this value the encoder counter will continue to count in the same direction when the motor is stopped.
- direction\_delay joint1, joint2, joint3, joint4 time delay (ms) after which the encoder count direction is reversed when the motor is stopped.

## 5.1.3.3 RA\_CTRL\_PARAMS

```
Parameter Set: RA CTRL PARAMS
mtr volt max
                   = [ 30
                              30
                                     30
                                           30
                   = [ 1
mtr volt min
                             1
                                   1
                                                ]
mtr volt init
                 0 ] =
                                  0
                                        0
                  = [ 0.013962 0.010908 0.017453 0.043633 ]
acc max
                 = [ 0.020944 0.016362 0.02618 0.06545 ]
vel max
vel min
                 0 ] =
                           0
                                 0
                                       0
                                   0.03
eps ioint
                 = [ 0.03
                            0.03
                                           0.05
                                                  1
deadband strt
                   = [ 3
                             3
                                    3
                                          3
                                                ]
deadband final via only = 1
                    = [ 0.001
                                0.001
                                        0.001
                                                0.001
deadband end
                                                        ]
                 = 0.4
eps time
                = [ 2750
                            3520
                                    2200
                                            880
p_gain
```

```
= [ 2291.7
i_gain
                             2933.3
                                      1833.3
                                               733.33
                 = [ 0
d gain
                           0
                                  0
                                        0
                                               1
filter p gain
                  = 0.0025
filter i gain
                 = 0.0127
loop time
                  = 0.1
loop time thermostat
loop time cooldown
                       = 0.2
delta via period
                    = 4
paci timeout
                   = 1000
stop to no op time delay = 5
power on time delay
off count
```

- mtr volt max joint1, joint2, joint3, joint4 max allowable motor voltage (volts).
- mtr volt min joint1, joint2, joint3, joint4 min allowable motor voltage (volts).
- mtr volt init joint1, joint2, joint3, joint4 volts applied to motor to start move (volts).
- acc\_max joint1, joint2, joint3, joint4 trapezoidal profile default accel(rad/s^2)
- vel max joint1, joint2, joint3, joint4 maximum joint velocity (rad/s)
- vel min joint1, joint2, joint3, joint4 minimum joint velocity (rad/s)
- eps\_joint joint1, joint2, joint3, joint4 when all joints get to within eps\_joint radians of their commanded via point, the next via point is sent to the RAE.
- deadband\_strt joint1, joint2, joint3, joint4 joint deadband at cmd start. Joint moves less than deadband\_strt will be ignored. Units are LSB of encoder counts or raw potentiometer reading depending on the joint sensor being used for ctrl (default is encoder).
- deadband\_final\_via\_only Bool for checking whether jnt is within deadband\_end of via point at final via point only (1) or for each via point (0)
- deadband\_end joint1, joint2, joint3, joint4 at cmd start. Final position that will be less than deadband end will be considered successful.
- eps\_time when all joints get to within *eps\_time* seconds of their commanded via point, the next via point is sent to the RAE. Applicable only to timed moves.
- p gain joint1, joint2, joint3, joint4 joint controller proportional gain (V/rad).
- i gain joint1, joint2, joint3, joint4 joint controller integral gain (V/sec).
- d gain joint1, joint2, joint3, joint4 joint controller derivative gain (Vsec/rad).
- filter p gain accommodation algorithm PI filter proportional gain.
- filter\_i\_gain accommodation algorithm PI filter integral gain.
- loop\_time controller sampling period (sec) for all commands except for the IDA THERMOSTAT command.
- loop\_time\_thermostat controller sampling period (sec) for the IDA\_THERMOSTAT command.
- loop time cooldown controller sampling period (sec) during actuator cooldown.
- delta\_via\_period period to send delta via (the change to the commanded via point) to RAE when the accommodation algorithm is executing.
- paci\_timeout timeout for paci communication to RAE (milliseconds).
- stop to no op time delay time delay for collecting final data after a stop command (sec).
- power\_on\_time\_delay time delay between eps power-on request and communicating with the RAE (sec).
- off\_count number of consecutive samples with motor power off before declaring move complete.

#### 5.1.3.4 RA\_LANDER\_TO\_RA

```
Parameter Set: RA_LANDER_TO_RA
frame.x = [ 0 0 0 ]
frame.q = [ 1 0 0 0 ]
```

- frame.x x, y, z of the RA base frame in the payload coordinate system (m).
- frame.q the unit quaternion representing the orientation transformation from the payload frame to the RA base frame. The identity is represented by [1 0 0 0].

#### 5.1.3.5 RA\_PATH\_PARAMS

```
Parameter Set: RA_PATH_PARAMS
path.cart.type = 0
path.cart.error = 0.01
path.cart.delta = 0.05
path.joint_delta = 0.085
path.time_delta = 5
```

- path.cart.type Type of motion.
  - $\circ$  0 straight-line motion.
  - $\circ$  1 joint-interpolation motion.
- path.cart.error allowable path error (m) for straight-line Cartesian motion.
- path.cart.delta allowable delta (m) between via points.
- path.joint\_delta allowable delta (rad) between via points for spatial joint moves.
- path.time\_delta allowable delta (sec) between via points for timed joint moves.

#### 5.1.3.6 RA\_TASK\_ALGO

```
Parameter Set: RA_TASK_ALGO

[op_code algo_code delta_via_code] = [ 11 3 3 ]

[op_code algo_code delta_via_code] = [ 18 3 3 ]

[op_code algo_code delta_via_code] = [ 18 3 3 ]

[op_code algo_code delta_via_code] = [ 22 1 2 ]

[op_code algo_code delta_via_code] = [ 47 3 3 ]

[op_code algo_code delta_via_code] = [ 48 3 3 ]

[op_code algo_code delta_via_code] = [ 49 2 3 ]

[op_code algo_code delta_via_code] = [ 0 0 0 ]

[op_code algo_code delta_via_code] = [ 0 0 0 ]

[op_code algo_code delta_via_code] = [ 0 0 0 ]

[op_code algo_code delta_via_code] = [ 0 0 0 ]

[op_code algo_code delta_via_code] = [ 0 0 0 ]
```

- op\_code the opcode for the command to which the algorithm applies. See rat\_show\_codes.
- algo code the control algorithm to be used during execution of the command with op code.
  - o 1 accommodate the arm will modify the trajectory in the direction of *delta\_via* (e.g., follow the surface with which it is in contact) when any joint torque exceeds *thresh\_a*.
  - $\circ$  2 contact the arm will stop on contact when any joint torque exceeds thresh c.
  - o 3 free space the arm will stop on contact when any joint torque exceeds thresh f.
- delta\_via\_code which *delta\_via* to use when the *accommodate* algorithm is active

- o 1 dig delta\_via is in direction orthogonal to the direction of motion, upward, and in the plane of the motion as determined by *ida trench angle*.
- 2 scrape delta\_via is orthogonal to, and upward from, the scraping plane found during IDA SCRAPE.
- o 3 user delta via user.

#### 5.1.3.7 RA ACT ALGO

```
Parameter Set: RA_ACT_ALGO
[op_code algo_code delta_via_code] = [ 17 2 3 ]
[op_code algo_code delta_via_code] = [ 19 2 3 ]
[op_code algo_code delta_via_code] = [ 20 3 3 ]
delta_via_user = [ 0 0 -1 ]
dvia_thresh = 0.01
```

- op code the opcode for the command to which the algorithm applies. See rat show codes.
- algo\_code the control algorithm to be used during execution of the command with op code op code.
  - o 1 accommodate the arm will modify the trajectory in the direction of *delta\_via* (e.g., follow the surface with which it is in contact) when any joint torque exceeds *thresh a*.
  - o 2 contact the arm will stop on contact when any joint torque exceeds thresh c.
  - o 3 free space the arm will stop on contact when any joint torque exceeds thresh f.
- delta via code which delta via to use when the accommodate algorithm is active
  - o 1 dig delta\_via is in direction orthogonal to the direction of motion, upward, and in the plane of the motion as determined by *ida trench angle*.
  - 2 scrape delta\_via is orthogonal to, and upward from, the scraping plane found during IDA SCRAPE.
  - o 3 user delta via user.
- delta via user − x, y, z
- dvia thresh threshold (magnitude of Cartesian delta via in m) at which accommodation begins.

#### 5.1.3.8 RA\_TAU\_PARAMS

```
Parameter Set: RA TAU PARAMS
limit
       = [ 26
                  91
                         53
                                10
         = [ 26
thresh a
                     91
                            53
                                   10
                                              ]
thresh c
          = [ 35
                     120
                            65
                                   10.5
thresh f
         = [ 35
                    120
                            65
                                   10.5
                      37.28
                              23.3
                                      9.32
thresh d
          = [ 29.125
       = [ 2
                        2
                               2
fit nl
                  2
         = [ 0.014134  0.016033  0.014041  0.0054075
c nl 0
c nl 1
         = [ 0.0021647 0.0008571 0.0007949 0.0078765
                                                          1
c nl 2
         = [ 0.028697  0.052189  0.052205  0.0078644
         = [ 0.0081567 0.0115545 0.009798 0.0041967
c nl 3
                                                         ]
c nl 4
         2525
                                     2525
temp.b
         = [ 2525
                     2525
                                             613.327 ]
temp.m
          = [ 0.2266
                      0.2259
                               0.2266
                                       0.2283
                                                0.4469 ]
                             30
mtr volt max = [30]
                      30
                                     30
```

• limit – joint1, joint2, joint3, joint4 joint torque limits (N-m) above which damage may occur.

- thresh\_a joint1, joint2, joint3, joint4 joint torque thresholds (N-m) for the accommodation algorithm.
- thresh\_c joint1, joint2, joint3, joint4 joint torque thresholds (N-m) for the contact algorithm.
- thresh\_f joint1, joint2, joint3, joint4 joint torque thresholds (N-m) for the free-space algorithm.
- thresh\_d joint1, joint2, joint3, joint4 detent torque in N-m added to threshold if actuator moving less than detent velocity.
- fit nl joint1, joint2, joint3, joint4 no-load current curve fit type
  - o 0 Polynomial fit
  - o 1 Exponential fit
  - o 2 Exponential fit w/ motor volt
- c nl 0 joint1, joint2, joint3, joint4 No-load current curve fit first coefficient
- c nl 1 joint1, joint2, joint3, joint4 No-load current curve fit second coefficient
- c nl 2 joint1, joint2, joint3, joint4 No-load current curve fit third coefficient
- c nl 3 joint1, joint2, joint3, joint4 No-load current curve fit forth coefficient
- c nl 4 joint1, joint2, joint3, joint4 No-load current curve fit fifth coefficient
- temp.b joint1, joint2, joint3, joint4 grapple temperature offset (LSBs). Value at which temperature is zero degrees Celsius.
- temp.m joint1, joint2, joint3, joint4, grapple temperature slope (Celsius/LSB).
- mtr\_volt\_max joint1, joint2, joint3, joint4 max motor volt in volts used during joint actuator characterization.

#### 5.1.3.9 RA\_TAU\_PARAMS2

```
Parameter Set: RA TAU PARAMS2
                                 110 ]
current limit = [ 110
                     260
                           210
torque limit = [ 35
                     120
                           65
                                 10.5
no load volt = [ 0
                     0
                          0
                                0
current delta = [ 1
                     1
                          1
                                1
tau detent = [ 29.125 37.28 23.3 9.32 ]
speed detent = [ 0.018  0.0098  0.0158  0.048 ]
fit ka
         = [ 1
                       1
                  1
                            1
c ka 0
           = [ 468.72 574.79 371.6 116.53 ]
           = [ 0
c ka 1
                    0
                         0
                              0
c ka 2
           = [ 0
                    0
                         0
                              0
           0 ] =
c ka 3
                    0
                         0
                              0
c_ka_4
           = [ 0
                              0
```

- current limit joint1, joint2, joint3, joint4 default current limits (mA).
  - o If current limit = -1 compute current limit autonomously.
- torque\_limit joint1, joint2, joint3, joint4 torque limit (N-m) for computing current limit as function of temperature.
- no\_load\_volt joint1, joint2, joint3, joint4 voltage (V) used with voltage-based no-load model (if selected) for computing current limit as function of temperature.
- current\_delta joint1, joint2, joint3, joint4 computed torque is zero if current is within +/-current delta (LSB) of current offset b.
- tau detent joint1, joint2, joint3, joint4 detent torque (N-m) for computing detent current.
- speed detent joint1, joint2, joint3, joint4 speed below which detent comes into play (rad/s).
- fit ka joint1, joint2, joint3, joint4 torque constant curve fit type.
  - $\circ$  0 Polynomial Fit
  - 1 Exponential Fit

- c ka 0 joint1, joint2, joint3, joint4 torque constant curve fit first coefficient
- c ka 1 joint1, joint2, joint3, joint4 torque constant curve fit second coefficient
- c ka 2 joint1, joint2, joint3, joint4 torque constant curve fit third coefficient
- c\_ka\_3 joint1, joint2, joint3, joint4 torque constant curve fit forth coefficient
- c ka 4 joint1, joint2, joint3, joint4 torque constant curve fit fifth coefficient

#### 5.1.3.10 RA\_SCIENCE\_DATA\_PERIOD

```
Parameter Set: RA_SCIENCE_DATA_PERIOD science data period = 1
```

• science\_data\_period - integer number of sampling periods between collection of each set of science data which are stored in heap.

#### 5.1.3.11 RA FAULT DETECT

```
Parameter Set: RA FAULT DETECT
enc pot delta
                = [ 0.1 0.1 0.1
                                        1
runaway joint delta = 0.1745
runaway pos delta = 0.1
runaway_ori_delta = 3.14
runaway time delta = 5
joint delta
             = [ 0.034 0.034 0.034 0.034 ]
vref nominal
               = [ 4.5 -4.5
                                      ]
vref delta
              = [ 0.03 0.03
                                     ]
enc delta
              = 2
              = 20
pot delta
tau
            = [ 10
                    29.2 17.2 3
motor samples
                 = 100
               = 1
current epsilon
heater time
               = [ 1200 1200 180
                                    180
               = [ 20 20
temp delta
                            20
                                 20
impeded samples
                  = [ 2
                          2
                               2
pot samples
                = 20
encoder samples
                  = 20
enc pot samples
                  = 2
vref samples
                = 3
runaway samples
kinematic samples = 2
heater rtd samples = 3
                           200
                                200
htr crnt
             = [ 120 80
                                       1
htr crnt offset = 2048
ace cal samples
power 30v samples = 10
stopped samples = 100
stalled samples = 100
deflection limit = 0.5
subtrench attempts = 2
dvia mag limit
                = 0.4
default cmd token = 1
collision mode
```

#### lander tol = 0.015

- enc\_pot\_delta joint1, joint2, joint3, joint4 allowable difference in radians between the joint angle computed from the encoder and the pot above which a fault is declared.
- runaway\_joint\_delta joint delta for a spatial joint move, if the difference in radians between the commanded and current joint angle is greater than runaway\_joint\_delta+ joint\_delta+eps\_joint, then a fault is declared.
- runaway\_pos\_delta position delta for a Cartesian move, if the difference in meters between the commanded and current Cartesian position is greater than *runaway\_pos\_delta*+ cart.delta, then a fault is declared.
- runaway\_ori\_delta orientation delta for a Cartesian move, if the difference in radians between the commanded and current orientation is greater than *runaway ori delta*, then a fault is declared.
- runaway\_time\_delta time delta for a timed joint move, if the difference in seconds between the current and commanded time is greater than runaway\_time\_delta+ time\_delta, then a fault is declared.
- joint\_delta joint1, joint2, joint3, joint4 joint delta where if a joint is commanded to move or moves within *joint delta* radians of its joint hard stop, then a kinematic fault is declared.
- vref nominal vref1, vref2 nominal values for the positive and negative voltage references.
- vref\_delta vref1, vref2 voltage delta where if a voltage reference differs from vref\_nominal by more than vref\_delta, then a fault is declared.
- enc\_delta encoder delta where if a motor is on and the encoder counter changes by less than enc\_delta counts between samples, then an encoder fault is declared.
- pot\_delta potentiometer delta where if a motor is on and the joint torque is less than *tau* and the pot changes by less than *pot delta* LSBs between samples, then an pot fault is declared.
- tau joint1, joint2, joint3, joint4 torque threshold for pot check (N-m).
- motor samples max allowable consecutive anomalies after which a motor fault is declared.
- current\_epsilon current in LSBs below *current\_epsilon* is considered to be zero. Used in motor, motor stall, and 30V power converter fault detection algorithms.
- heater\_time heater time for when a heater is turned on, the heating rate is checked after heater time seconds elapses.
  - o Element 0 is for joint 1, 2, and 3 heaters
  - o Element 1 is for joint 4 heater
  - o Element 2 is for grapple heater 1
  - o Element 3 is for grapple heater 2
- temp\_delta temperature delta for when a heater is turned on, if the joint temperature (i = 0, 3) has not risen by temp\_delta LSBs in heater\_time seconds, then a heater or temperature sensor fault is declared.
  - o Element 0 is for joint 1
  - o Element 1 is for joint 2
  - o Element 2 is for joint 3
  - o Element 3 is for joint 4
  - o Element 4 is for the grapple
- impeded\_samples joint1, joint2, joint3, joint4 max allowable consecutive anomalies after which a motion-impeded event is declared.
- pot samples max allowable consecutive anomalies after which a pot fault is declared.
- encoder\_samples max allowable consecutive anomalies after which an encoder fault is declared.
- enc\_pot\_samples max allowable consecutive anomalies after which an encoder-pot delta fault is declared.

- vref\_samples max allowable consecutive anomalies after which a voltage reference fault is declared.
- runaway\_samples max allowable consecutive anomalies after which a joint runaway fault is declared.
- kinematic\_samples max allowable consecutive anomalies after which a kinematic fault is declared.
- heater\_rtd\_samples max allowable consecutive anomalies after which a heater or temperature sensor fault is declared.
- htr\_crnt if a heater is turned on and the heater current in LSBs is less than htr\_crnt, then a heater/sensor fault is declared. Also used in the 30V power supply fault detection algorithm.
  - o Element 0 is for joint 1, 2, and 3 heaters
  - o Element 1 is for joint 4 heater
  - o Element 2 is for grapple heater 1
  - o Element 3 is for grapple heater 2
- htr crnt offset zero heater current in LSBs.
- ace\_cal\_samples max allowable consecutive anomalies after which an A/D converter calibration fault is declared.
- power\_30V\_samples max allowable consecutive anomalies after which a 30V power converter fault is declared.
- stopped\_samples max allowable consecutive anomalies after which a premature motion termination fault is declared.
- stalled\_samples max allowable consecutive anomalies after which a motor stalled fault is declared.
- deflection\_limit max allowable joint delta between deflected and undeflected pose (RSS) in radians.
- subtrench\_attempts max allowable attempts at digging the same subtrench before issuing fault.
- dvia mag limit max allowable delta via (m).
- default\_cmd\_token default command ID token for RA\_SEND\_DATA. Used primarily for sending of ra history data when a fault occurs.
- collision mode mode used for calculation of link poses in collision detection:
  - $\circ$  0 collision detection off.
  - $\circ$  1 No deflection compensation in collision detection.
  - 2 Use deflection compensation in collision detection.
- lander\_tol the tolerance to add around each lander object whose individual tolerance is not specified for detecting collisions in m.

#### 5.1.3.12 RA\_TASK\_C

```
Parameter Set: RA_TASK_C
calibrate.home = [-3.313 -2.21 -0.401 0.2]
calibrate.angle = [ 0.2  0.2  0.2  0.2 ]
calibrate.current = [ 30  120  40  18 ]
calibrate.time = [ 40  40  40  40 ]
calibrate.delta = [ 0  0  0  0 ]
```

- calibrate.home joint1, joint2, joint3, joint4 staging angles if call to IDA\_CALIBRATE is set with the enum RA\_NEG\_HARDSTOP as argument for each joint.
- calibrate.angle joint1, joint2, joint3, joint4 angles from the hard stop the joints will move to prior to the timed moves that calibrate the arm.

- calibrate.current Obsolete. The current limits are set autonomously at the actuator command level.
- calibrate.time joint1, joint2, joint3, joint4 times in seconds of timed moves which run joints up against hard stops.
- calibrate.delta joint1, joint2, joint3, joint4 difference in radians between pot and encoder at hard stops. It is added to the hard stop joint angle computed from the pots prior to setting the encoder counters. *delta* compensates for the windup in the drive train which occurs when the joints run up against the hard stops.

#### 5.1.3.13 **RA\_TASK\_DT**

```
Parameter Set: RA TASK DT
dig trench.height
                        = -0.2
dig trench.[depth width length] = [ 0.002 0.073 0.25]
dig trench.corner
                        = 0.15
dig trench.scoop angle
                           = 0.125
dig trench.carry angle
                           = 2.5
dig trench.dump angle
                            = 7.7125
dig trench.return angle
                           = 2
dig trench.way point
                          = [ 0.1  0.1  0  ]
```

- dig\_trench.height height in meters above the starting commanded position to where the scoop is initially moved. It is added to <u>ra\_pos\_z</u>.
- dig\_trench.depth the depth in meters of a single subtrench. If this parameter is less than or equal to the trench\_depth specified in the command, then more than one subtrench in depth will be dug.
- dig\_trench.width the width in meters of a single subtrench. If this parameter is less than or equal to the <u>trench\_width</u> specified in the command, then more than one subtrench in width will be dug. Note that the width of the scoop is 0.073m.
- dig\_trench.length the length in meters of a single subtrench. The number of subtrenches dug in length at each depth is a function of trench\_length, trench\_depth, dig\_angle1, dig\_angle2, and depth.
- dig\_trench.corner length in meters of the corner motion. The corner motion is the translation and rotation that the scoop makes from the entry ramp to the trench bottom and the from the trench bottom to the exit ramp. If the length of the subtrench is less than the corner motion, then the corner motion from the entry ramp to the trench bottom is proportionally reduced by corner/subtrench\_length in both translation and rotation. The full corner motion is always executed from the bottom of the trench to the exit ramp. The parameter should be large enough so that the corner motion can complete without the back of the scoop hitting the entry ramp during the move from the entry ramp to the trench bottom or hitting the trench bottom during the move from trench bottom to the exit ramp. The default value is 0.15m.
- dig\_trench.scoop\_angle planning angle for the scoop in radians. It is the angle from the direction of motion of the scoop to the scoop frame approach (z) vector during digging motions (entry ramp, trench bottom, exit ramp).
- dig\_trench.carry\_angle scoop angle in radians during the move from the exit of the subtrench to the dump position.
- dig\_trench.dump\_angle scoop angle in radians after dumping the contents.
- dig trench.return angle scoop angle in radians upon returning to way point post-dump.
- dig\_trench.way\_point x, y, z intermediate position expressed relative to the <u>dump position</u> in meters through which the scoop passes enroute from the exit of the subtrench to the dump position.

#### 5.1.3.14 RA\_TASK\_SC

```
Parameter Set: RA_TASK_SC
scrape.guard_angle = 1.629
scrape.guard_depth = 0.1
scrape.rake = [ 0 0 1.5368]
scrape.backoff = 0.06
scrape.height_initial = 0
```

- scrape.guard\_angle scoop angle in radians for the guarded move.
- scrape.guard depth attempted depth in meters of the guarded move.
- scrape.rake blade1, blade2, scoop rake angle in radians.
- scrape.backoff distance in meters to back away from the surface prior to each scraping motion to allow set up to the other tool.
- scrape.height\_initial initial height in meters above the surface where the tool is placed prior to initiation of the scraping motion.

#### 5.1.3.15 RA COMPRESS PARAMS

```
Parameter Set: RA_COMPRESS_PARAMS
compress.wSyncInterval = 1024
compress.wBlockSize = 16
compress.wSegmentSize = 1024
compress.type = 0
```

- scrape.wSyncInterval sync interval length used in Golomb-Rice encoding algorithm.
- scrape.wBlockSize block size used in Golomb-Rice encoding algorithm.
- scrape.wSegmentSize segment size used in Golomb/Rice encoding algorithm.
- scrape.type Not used. All compression is Golomb-Rice

#### **5.1.3.16** RA MAX FAULTS

```
Parameter Set: RA MAX FAULTS
max fault.ace reset
                      = 0
max fault.motion impeded = 4
max fault.file io
                   = 0
                   = 0
max fault.paci
max fault.tv power
                      = 0
max fault.stopped
                     = 3
max fault.stalled
                    = 3
max fault.overheat
                     = 3
```

- max fault.ace reset number of allowed micro-processor reset faults before safing the RA.
- max\_fault.motion\_impeded number of allowed arm movement obstructed faults before safing the RA.
- max fault.file io number of allowed reading or writing to a file faults before safing the RA.
- max fault.paci number of allowed no communications the RAE faults before safing the RA.
- max\_fault.tv\_power number of allowed 30V power supply fault faults before safing the RA.

- max\_fault.stopped number of allowed premature motion termination faults before safing the RA.
- max fault.stalled number of allowed motor stalled faults before safing the RA.
- max\_fault.overheat number of allowed actuator over heat faults before safing the RA.

#### 5.1.3.17 RA\_FAULT\_PARAMS

```
Parameter Set: RA FAULT PARAMS
fault params.dt backup
                                = 0.03
fault params.scr initial
                              = 0.005
fault params.scr delta
                               = 0.001
fault params.scr total
                              = 0.003
fault params.ignore col blade 1
                                    = 0
fault params.ignore col blade 2
                                   = 0
fault params.ignore col rac
                                 = 0
                                   = 0
fault params.ignore col scoop
fault params.ignore col wrist
                                 = 0
fault params.ignore col grapple attach = 0
fault params.ignore col grapple
                                   = 0
fault params.ignore col seis
                                 = 0
                                 = 0
fault params.ignore col wts
fault params.ignore col hp3
                                  = 0
```

- fault\_params.dt\_backup distance in meters to move scoop away from trench when recovering from a motion-impeded event during <u>IDA\_DIG\_TRENCH</u>.
- fault\_params.scr\_initial distance to move to in meters from trouble spot as setup position for scraping. (not used)
- fault params.scr delta change in meters in depth for each successive scrape. (not used)
- fault\_params.scr\_total total change in meters in depth at which point scraping is terminated. (not used)
- fault params.ignore col blade 1 ignore collision mask forward-facing scraping blade.
- fault params.ignore col blade 2 ignore collision mask backward-facing scraping blade.
- fault params.ignore col rac boolean to ignore collision mask rac.
- fault params.ignore col scoop boolean to ignore collision mask scoop blade.
- fault params.ignore col wrist boolean to ignore collision mask wrist.
- fault params.ignore col grapple attach boolean to ignore collision mask grapple-attach.
- fault params.ignore col grapple boolean to ignore collision mask grapple.
- fault params.ignore col seis boolean to ignore collision mask SEIS.
- fault params.ignore col wts boolean to ignore collision mask WTS.
- fault params.ignore col hp3 boolean to ignore collision mask HP3.

#### 5.1.3.18 RA POWER STATES

```
Parameter Set: RA_POWER_STATES
power_states.power = [ 11 18 43]
eps_switch = 0
```

• power\_states.power - RA\_POWER\_IDLE state, RA\_POWER\_HEAT state, RA\_POWER\_MOVING state power value for each state in Watts.

• eps switch - whether to use primary or secondary EPS switch. 0 for primary, 1 for secondary.

#### **5.1.3.19 RA GRAVITY**

```
Parameter Set: RA_GRAVITY
gravity_params.acc_g = 3.711
gravity_params.grav_vect = [0.046825 -0.051123 0.997594]
```

- gravity\_params.acc\_g gravitational acceleration magnitude (m/s^2).
- gravity\_params.grav\_vect x, y, z gravitational vector in payload frame.

#### 5.1.3.20 RA DEFL GENERAL

```
Parameter Set: RA_DEFL_GENERAL

defl_params.enable_abs = 1

defl_params.enable_rel = 0

defl_params.enable_tool = 0

defl_params.enable_jint_abs = 0

defl_params.enable_jint_rel = 0

seis_mass = 8.900000

wts_mass = 7.300000

hp3_mass = 2.700000

compliance_scale = 1.092301
```

- defl\_params.enable\_abs boolean to enable deflection compensation algorithm for Cartesian moves.
- defl\_params.enable\_rel boolean to enable deflection compensation algorithm for relative Cartesian moves. (Not implemented)
- defl\_params.enable\_tool boolean to enable deflection compensation algorithm for tool-frame Cartesian moves. (Not implemented)
- defl\_params.enable\_jnt\_abs boolean to enable deflection compensation algorithm for absolute joint moves. (Not implemented)
- defl\_params.enable\_int\_rel boolean to enable deflection compensation algorithm for relative joint moves. (Not implemented)
- seis mass mass of the SEIS instrument in kilograms.
- wts\_mass mass of the WTS instrument in kilograms.
- hp3 mass mass of the HP3 instrument in kilograms.
- compliance scale scaling factor for compliance parameters.

#### 5.1.3.21 RA\_DEFL\_LINK\_0 – Arm Base

```
3.290000e-24 2.430000e-25 4.560000e-24
9.160000e-24 6.570000e-24 4.230000e-25]

vCm = [ 3.020000e-25 4.940000e-24 7.990000e-24
-3.060000e-24 3.750000e-25 7.010000e-24
4.930000e-25 5.290000e-24 -8.830000e-26]

wCm = [ 8.850000e-08 -2.280000e-25 7.170000e-24
1.050000e-23 8.850000e-08 -5.630000e-24
7.840000e-24 -6.390000e-24 8.850000e-08]
```

- mass lumped mass for the link in kilograms.
- cm x x coordinate of the center of mass for the link.
- cm y y coordinate of the center of mass for the link.
- cm\_z z coordinate of the center of mass for the link.
- vCf 9 values representing the 3x3 vCf component of the compliance matrix. These are in row-major order.
- wCf 9 values representing the 3x3 wCf component of the compliance matrix. These are in row-major order.
- vCm 9 values representing the 3x3 vCm component of the compliance matrix. These are in row-major order.
- wCm 9 values representing the 3x3 wCm component of the compliance matrix. These are in row-major order.

#### 5.1.3.22 RA\_DEFL\_LINK\_1 - Azimuth

```
Parameter Set: RA DEFL LINK 1
mass = 0.509
cm x = 0.025
cm_y = 0.0579
cm z = -0.0556
vCf = [ 3.840000e-08 2.310000e-08 -2.730000e-21
      2.310000e-08 2.250000e-08 -2.010000e-21
     -4.050000e-21 -2.900000e-21 3.060000e-07 ]
wCf = [ 9.620000e-22 -5.420000e-09 -8.470000e-07
      5.420000e-09 1.060000e-19 -9.820000e-06
      8.470000e-07 6.030000e-07 -7.470000e-20 1
vCm = [-2.520000e-20 5.420000e-09 8.470000e-07
     -5.420000e-09 9.950000e-20 6.030000e-07
     -8.470000e-07 -9.820000e-06 -1.050000e-19]
wCm = [ 2.220000e-05 5.130000e-18 1.820000e-20
      6.060000e-18 3.603190e-04 3.840000e-18
     -6.660000e-19 3.670000e-18 2.220000e-05]
```

- mass lumped mass for the link in kilograms.
- cm x x coordinate of the center of mass for the link.
- cm y y coordinate of the center of mass for the link.
- cm z z coordinate of the center of mass for the link.
- vCf 9 values representing the 3x3 vCf component of the compliance matrix. These are in row-major order.
- wCf 9 values representing the 3x3 wCf component of the compliance matrix. These are in row-major order.

- vCm 9 values representing the 3x3 vCm component of the compliance matrix. These are in row-major order.
- wCm 9 values representing the 3x3 wCm component of the compliance matrix. These are in row-major order.

#### 5.1.3.23 RA DEFL LINK 2 – Upper Arm

```
Parameter Set: RA DEFL LINK 2
mass = 1.2381
cm x = 0.708
cm y = 0
cm z = -0.0762
vCf = [ 6.180000e-06 -4.110000e-06 6.530000e-05
     -4.110000e-06 1.730570e-04 5.340000e-07
      6.530000e-05 5.340000e-07 7.940660e-04 1
wCf = [-3.250000e-07 8.270000e-05 7.000000e-06]
     -7.690000e-05 3.250000e-07 -8.573120e-04
     -6.870000e-06 2.152100e-04 -6.990000e-12 ]
vCm = [-3.250000e-07 -7.690000e-05 -6.870000e-06]
      8.270000e-05 3.250000e-07 2.152100e-04
      7.000000e-06 -8.573120e-04 -6.990000e-12 ]
wCm = [ 1.085949e-03 4.260000e-06 -4.010000e-09
      4.260000e-06 1.008957e-03 -2.210000e-10
     - 4.010000e-09 -2.210000e-10 3.512170e-04]
```

- mass lumped mass for the link in kilograms.
- cm x x coordinate of the center of mass for the link.
- cm y y coordinate of the center of mass for the link.
- cm z z coordinate of the center of mass for the link.
- vCf 9 values representing the 3x3 vCf component of the compliance matrix. These are in row-major order.
- wCf 9 values representing the 3x3 wCf component of the compliance matrix. These are in row-major order.
- vCm 9 values representing the 3x3 vCm component of the compliance matrix. These are in row-major order.
- wCm 9 values representing the 3x3 wCm component of the compliance matrix. These are in row-major order.

#### 5.1.3.24 RA DEFL LINK 3 STOWED – Forearm (w/ Grapple stowed)

```
5.940000e-28 3.824210e-04 -4.240000e-24 ]
vCm = [-4.290000e-31 5.950000e-08 -3.390000e-26
-5.870000e-08 3.540000e-24 3.824210e-04
6.670000e-29 -1.275284e-03 1.940000e-26 ]
wCm = [ 1.969914e-03 -1.120000e-21 9.440000e-09
-9.370000e-29 1.791046e-03 -2.440000e-26
9.440000e-09 5.300000e-24 7.513490e-04 ]
```

- mass lumped mass for the link in kilograms.
- cm x x coordinate of the center of mass for the link.
- cm y y coordinate of the center of mass for the link.
- cm z z coordinate of the center of mass for the link.
- vCf 9 values representing the 3x3 vCf component of the compliance matrix. These are in row-major order.
- wCf 9 values representing the 3x3 wCf component of the compliance matrix. These are in row-major order.
- vCm 9 values representing the 3x3 vCm component of the compliance matrix. These are in row-major order.
- wCm 9 values representing the 3x3 wCm component of the compliance matrix. These are in row-major order.

#### 5.1.3.25 RA\_DEFL\_LINK\_3\_UNSTOWED – Forearm (w/ Grapple Unstowed)

```
Parameter Set: RA DEFL LINK 3 UNSTOWED
mass = 1.4944
cm x = 0.481
cm_y = 0.031
cm z = -0.017
vCf = [ 1.020000e-07 -1.720000e-26 -4.830000e-08
     3.940000e-28 2.526130e-04 -2.830000e-24
    -4.830000e-08 9.850000e-27 1.019379e-03]
wCf = [-4.220000e-26 -5.870000e-08 8.920000e-22]
     5.950000e-08 -1.240000e-26 -1.275284e-03
     5.940000e-28 3.824210e-04 -4.240000e-24 1
vCm = [-4.290000e-31 5.950000e-08 -3.390000e-26
    -5.870000e-08 3.540000e-24 3.824210e-04
     6.670000e-29 -1.275284e-03 1.940000e-26 ]
wCm = [ 1.969914e-03 -1.120000e-21 9.440000e-09
    -9.370000e-29 1.791046e-03 -2.440000e-26
     9.440000e-09 5.300000e-24 7.513490e-04]
```

- mass lumped mass for the link in kilograms.
- cm x x coordinate of the center of mass for the link.
- cm\_y y coordinate of the center of mass for the link.
- cm z z coordinate of the center of mass for the link.
- vCf 9 values representing the 3x3 vCf component of the compliance matrix. These are in row-major order.
- wCf 9 values representing the 3x3 wCf component of the compliance matrix. These are in row-major order.

- vCm − 9 values representing the 3x3 vCm component of the compliance matrix. These are in row-major order.
- wCm 9 values representing the 3x3 wCm component of the compliance matrix. These are in row-major order.

#### 5.1.3.26 RA\_DEFL\_LINK\_4\_STOWED – Wrist (w/ Grapple stowed)

```
Parameter Set: RA DEFL LINK 4 STOWED
mass = 0.1481
cm x = 0.0114
cm y = -0.0673
cm z = -0.008
vCf = [ 5.710000e-09 -2.160000e-17 1.840000e-18
     -2.160000e-17 5.710000e-09 2.650000e-18
      1.840000e-18 2.650000e-18 5.710000e-09]
wCf = [-1.220000e-35 -6.090000e-13 -2.140000e-10
      1.830000e-11 -2.150000e-37 1.490000e-10
      2.140000e-10 -4.960000e-12 9.290000e-36 ]
vCm = [-1.160000e-35 1.830000e-11 2.140000e-10
     -6.090000e-13 2.340000e-36 -4.960000e-12
     -2.140000e-10 1.490000e-10 1.240000e-35 ]
wCm = [4.930000e-05-9.850000e-28-0.000000e+00]
     -9.850000e-28 1.475213e-03 1.230000e-28
     1.280000e-31 9.770000e-29 4.930000e-05 l
```

- mass lumped mass for the link in kilograms.
- cm x x coordinate of the center of mass for the link.
- cm y y coordinate of the center of mass for the link.
- cm z z coordinate of the center of mass for the link.
- vCf 9 values representing the 3x3 vCf component of the compliance matrix. These are in row-major order.
- wCf 9 values representing the 3x3 wCf component of the compliance matrix. These are in row-major order.
- vCm 9 values representing the 3x3 vCm component of the compliance matrix. These are in row-major order.
- wCm 9 values representing the 3x3 wCm component of the compliance matrix. These are in row-major order.

#### 5.1.3.27 RA DEFL LINK 4 UNSTOWED – Wrist (w/ Grapple Unstowed)

- mass lumped mass for the link in kilograms.
- cm x x coordinate of the center of mass for the link.
- cm\_y y coordinate of the center of mass for the link.
- cm z z coordinate of the center of mass for the link.
- vCf 9 values representing the 3x3 vCf component of the compliance matrix. These are in row-major order.
- wCf 9 values representing the 3x3 wCf component of the compliance matrix. These are in row-major order.
- vCm − 9 values representing the 3x3 vCm component of the compliance matrix. These are in row-major order.
- wCm 9 values representing the 3x3 wCm component of the compliance matrix. These are in row-major order.

#### 5.1.3.28 **RA\_DEFL\_LINK\_5 – Tool**

```
Parameter Set: RA DEFL LINK 5
mass = 0
cm x = 0
cm y = 0
cm z = 0
vCf = [0.000000e+00 0.000000e+00 0.000000e+00]
     0.000000e+00 0.000000e+00 0.000000e+00
     0.000000e+00 0.000000e+00 0.000000e+00]
wCf = [0.000000e+00 0.000000e+00 0.000000e+00]
     0.000000e+00 0.000000e+00 0.000000e+00
     0.000000e+00 0.000000e+00 0.000000e+001
vCm = [0.000000e+00 0.000000e+00 0.000000e+00]
     0.000000e+00 0.000000e+00 0.000000e+00
     0.000000e+00 0.000000e+00 0.000000e+001
wCm = [0.000000e+00 0.000000e+00 0.000000e+00]
     0.000000e+00 0.000000e+00 0.000000e+00
     0.000000e+00 0.000000e+00 0.000000e+001
```

- mass lumped mass for the link in kilograms.
- cm x x coordinate of the center of mass for the link.
- cm y y coordinate of the center of mass for the link.
- cm z z coordinate of the center of mass for the link.
- vCf 9 values representing the 3x3 vCf component of the compliance matrix. These are in row-major order.
- wCf 9 values representing the 3x3 wCf component of the compliance matrix. These are in row-major order.

- vCm 9 values representing the 3x3 vCm component of the compliance matrix. These are in row-major order.
- wCm 9 values representing the 3x3 wCm component of the compliance matrix. These are in row-major order.

#### 5.1.3.29 **RA\_THERMAL**

```
Parameter Set: RA THERMAL
             = [-55
                             -55
                                   -55
temp min
                      -55
                                          -551
                       20
                             20
                                    20
temp delta
             = [ 20
                                          20 ]
temp max rotor = [ 95
                         95
                                95
                                      95
temp max case = [ 75
                          75
                                75
                                       75
temp cooldown = [ 45
                                45
                          45
                                      45
           = [ 0.1014  0.1014  0.1014  0.1014
CM r
R rtc
          = [ 0.0885  0.0885  0.0885  0.0885
l nl
         800.0] =
                    0.008 0.008 0.008
                                  42
R cal
          = [ 42
                     42
                           42
T cal
          = [ 20
                     20
                           20
                                 20
          = [ 0.00393 0.00393 0.00393 0.00393
alpha
filter alpha = 0.05
filter dt
          = 900
filter c 0
           = 4.429
           = 0.154
filter c 1
           = 0
filter c 2
filter c 3
           = 0
           = 0
filter c 4
```

- temp\_min joint1, joint2, joint3, joint4, unused joint temperature (Celsius) below which the FSW will turn on heaters to warm up actuators during motion or during execution of the <a href="IDA\_THERMOSTAT">IDA\_THERMOSTAT</a> command. If an actuator is not up to temperature when a move command is issued, motion is not initiated until the joint warms up. If a temperature sensor or heater fails, set temp min to -800 Celsius. Otherwise, motion will not be initiated.
- temp\_delta joint1, joint2, joint3, joint4, unused joint temperature delta (Celsius). Above temp\_min + temp\_delta the actuator heaters are turned off if they are on.
- temp\_max\_rotor joint1, joint2, joint3, joint4 joint actuator rotor temperature upper limit (Celsius). Computed from case temperature using thermal model.
- temp\_max\_case joint1, joint2, joint3, joint4 joint actuator case temperature upper limit (Celsius). Measured from PRTs.
- temp\_cooldown joint1, joint2, joint3, joint4 temperature to reach during cool down before resuming motion (Celsius).
- CM r joint1, joint2, joint3, joint4 rotor thermal mass (joules/ Celsius).
- R rtc joint1, joint2, joint3, joint4 1/(rotor-to-case thermal resistance) (watts/ Celsius).
- Inl-joint1, joint2, joint3, joint4 motor no-load current (A).
- R\_cal joint1, joint2, joint3, joint4 rotor resistance at cal temp (ohms).
- T cal joint1, joint2, joint3, joint4 cal temp (Celsius).
- alpha joint1, joint2, joint3, joint4 temperature coefficient of resistance of copper (ohms/Celsius).
- filter\_alpha weighting coefficient for ISAD rasp motor temperature filter.
- filter dt reseed the filter if it has been longer than *filter dt* since the last measurement.
- filter c 0 ISAD rasp motor temperature correction 0th order coefficient.
- filter c 1 ISAD rasp motor temperature correction 1st order coefficient.

- filter c 2 ISAD rasp motor temperature correction 2nd order coefficient.
- filter c 3 ISAD rasp motor temperature correction 3rd order coefficient.
- filter c 4 ISAD rasp motor temperature correction 4th order coefficient.

### 5.1.3.30 RA\_GRAPPLE\_PARAMS

```
Parameter Set: RA_GRAPPLE_PARAMS
grapple_heater = 1
max_temperature = 106.0
overheat_persistence = 2
limit_switch_persistence = 2
```

- grapple\_heater which grapple heater to use.
  - o 1 Grapple heater 1 only
  - o 2 Grapple heater 2 only
  - o 3 Both grapple heaters
- max temperature maximum allowed grapple actuator temperature (Celsius).
- overheat\_persistence number of consecutive times a grapple temperature must exceed the *max temperature* parameter before a grapple overheat fault is declared.
- limit\_switch\_persistence number of consecutive times the fingers-open limit switch must read tripped before the grapple opening algorithm will consider the fingers fully open.

#### 5.1.3.31 RA\_ACTIVE\_HOLD\_PARAMS

```
Parameter Set: RA_ACTIVE_HOLD_PARAMS
active_hold = 0
hold_time = 5.0
move time multiple = 2.0
```

- active\_hold whether to do active hold moves. 1.0 = Yes. Any other value means not to do active hold.
- hold time number of seconds to actively hold the position after completing an active hold move.
- move\_time\_multiple duration of each individual timed move in an active hold move, expressed as a multiple of the control loop time (loop\_time parameter in the <u>Control group</u>).

#### 5.1.3.32 PAYLOAD\_COL\_PARAMS

```
Parameter Set: PAYLOAD_COL_PARAMS  \begin{aligned} &\text{seis\_q\_(i,j,k,r)} = [ \ 0.000000 \ \ 0.000000 \ \ 0.177944 \ \ 0.984041 \ ] \\ &\text{seis\_t\_(x,y,z)} = [ \ -0.408000 \ \ -0.319000 \ \ -0.334000 \ \ ] \\ &\text{wts\_q\_(i,j,k,r)} = [ \ 0.000000 \ \ 0.000000 \ \ 1.0000000 \ \ ] \\ &\text{wts\_t\_(x,y,z)} = [ \ -0.996000 \ \ -0.459000 \ \ -0.261000 \ \ \ ] \\ &\text{hp3\_q\_(i,j,k,r)} = [ \ 0.000000 \ \ 0.000000 \ \ -0.175796 \ \ 0.984427 \ ] \\ &\text{hp3\_t\_(x,y,z)} = [ \ -0.861000 \ \ -0.008000 \ \ -0.455000 \ \ \ ] \end{aligned}
```

• seis\_q\_(i,j,k,r) – SEIS quaternion vector from the lander frame to the static SEIS collision link frame.

```
o seis_q_i - x * \sin(\frac{1}{2})
o seis q j - y * \sin(\frac{1}{2})
```

```
o seis_q_k - z * sin(theta/2)
o seis q r - cos(theta/2)
```

- seis\_t\_(x,y,z) x, y, z translation component from the lander frame to the static SEIS collision link frame.
- wts\_q\_(i,j,k,r) WTS quaternion vector from the lander frame to the static WTS collision link frame.

```
    wts_q_i - x * sin(theta/2)
    wts_q_j - y * sin(theta/2)
    wts_q_k - z * sin(theta/2)
    wts_q r - cos(theta/2)
```

- wts\_t\_(x,y,z) x, y, z translation component from the lander frame to the static WTS collision link frame.
- hp3\_q\_(i,j,k,r) HP3 quaternion vector from the lander frame to the static HP3 collision link frame.

```
\begin{array}{ll} \circ & wts\_q\_i-x * sin(theta/2) \\ \circ & wts\_q\_j-y * sin(theta/2) \\ \circ & wts\_q\_k-z * sin(theta/2) \\ \circ & wts\_q\_r-cos(theta/2) \end{array}
```

• hp3\_t\_(x,y,z) – x, y, z translation component from the lander frame to the static HP3 collision link frame.

## 5.1.4 IDA Position in Spacecraft Coordinates

The IDA position in spacecraft coordinates file contains the Cartesian coordinates (x\_coord(mm), y\_coord(mm), z\_coord(mm)) of the Lander Mechanical frame origin relative to the Payload frame. The file name is: ida sc coordinates.csv

## 5.1.5 Engineering/Science High Priority (SciHi) Data

Science High Priority data is non-channelized telemetry science data that is sent to the *high* priority APID (87). The data is collected after the previous data dump command is executed. Note that the previous data dump command sent science data to telemetry on that day and cleared the buffer for new data. It contains detailed sensor data typically collected every sample period and is used for reconstruction of IDA performance. The timestamp represents the last time IDA MC data was received.

The Science High Priority (SciHi) data product is a .csv file with parameter values described in Table 12. In each description, a snapshot of the parameter from the .csv file in excel is shown. The RA\_DOF is a set that represents the 4 degrees of freedom of the IDA: shoulder yaw (azimuth), shoulder (elevation), elbow, and wrist pitch. Assume in IDA frame.

| Name (in .csv)                                   | Units   | Description             | Snapshot of .csv in Excel  |
|--|---------|-------------------------|--|
| time(s)  | second  | time readings recorded  | #time(s)<br>42209.8  |
| enc1(rad)<br>enc2(rad)<br>enc3(rad)<br>enc4(rad) | radians | encoder counts [RA_DOF] | enc1(rad) enc2(rad) enc3(rad) enc4(rad) -2.84 -1.9231 2.3173 -0.0007 |

Table 12 - Science data parameters

| pot1(rad)       |                 |   |              |             |            |             |
|-----------------|-----------------|---|--------------|-------------|------------|-------------|
| pot2(rad)       | potentiometer   |   | pot1(rad)    | pot2(rad)   | pot3(rad)  | pot4(rad)   |
| pot3(rad)       | radians         | measurement [RA DOF]                            | -2.8391      | -1.9224     | 2.320      |             |
| pot4(rad)       |                 |   |              |             |            |             |
| tcase1(C)       |                 |   |              |             |            |             |
| tcase2(C)       | Celsius         | measured motor case                             | enc1(rad)    | enc2(rad)   | enc3(rad)  | enc4(rad)   |
| tcase3(C)       | Ceisius         | temp [RA_DOF]                                   | -2.84        | -1.9231     | 2.317      | -0.0007     |
| tcase4(C)       |                 |   | 1            |             |            |             |
| trotor1(C)      |                 |   |              |             |            |             |
| trotor2(C)      | Celsius         | computed motor rotor                            | trotor1(C)   | trotor2(C)  | trotor3(C) | trotor4(C)  |
| trotor3(C)      | Ceisius         | temperature [RA_DOF]                            | -52.2227     | -52.7207    | -50.087    | 72 -51.1683 |
| trotor4(C)      |                 |   |              |             |            |             |
| tarannla(C)     | Celsius         | mater temperature                               | tgrapple(C)  |             |            |             |
| tgrapple(C)     | Ceisius         | motor temperature                               | -26.9399     |             |            |             |
| cur1(mA)        |                 |   |              |             |            |             |
| cur2(mA)        | :11:            | motor currents                                  | cur1(mA)     | cur2(mA)    | cur3(mA)   | cur4(mA)    |
| cur3(mA)        | milliampere     | [RA_DOF]  | 0            | -0.3125     | -0.312     | -0.3125     |
| cur4(mA)        |                 |   |              |             |            | -           |
| volt1(V)        |                 |   |              |             |            |             |
| volt2(V)        | volt            | motor voltages                                  | volt1(V)     | volt2(V)    | volt3(V)   | volt4(V)    |
| volt3(V)        | voit            | [RA_DOF]  | 0            | 0           |            | 0 0         |
| volt4(V)        |                 |   |              |             |            |             |
| 4.4             | ,               | bit-mapped status word                          | stat         |             |            |             |
| stat            | n/a             | (Table 13)                                      | 0            |             |            |             |
|                 |                 | currently selected tool                         | tool         |             |            |             |
| tool            | n/a             | (Table 14)                                      | 5            |             |            |             |
|                 |                 | location of tool as                             | ,            |             |            |             |
| x_enc(m)        |                 | Cartesian coordinates in                        | x_enc(m)     | y_enc(m)    | z_enc(m)   |             |
| y_enc(m)        | meter           | IDA frame using joint                           | 1.3633       | 0.0043      | 0.493      | ) F         |
| z_enc(m)        |                 | encoder readings                                | 1.3033       | 0.0043      | 0.45       | 55          |
|                 |                 | orientation of tool in IDA                      | +            | r           |            |             |
| th_enc(m)       | radian          | frame using joint encoder                       | th_enc(m)    |             |            |             |
| tii_ene(iii)    | radian          | readings  | 1.5014       |             |            |             |
|                 |                 | location of tool as                             |              |             |            |             |
| x_pot(m)        |                 | Cartesian coordinates in                        | x_pot(m)     | y_pot(m)    | z_pot(m)   |             |
| y_pot(m)        | meter           | IDA frame using joint                           | 1.3585       | 0.0026      | 0.50       | 34          |
| z_pot(m)        |                 | potentiometer readings                          | 1.5505       | 0.0020      | 0.50       |             |
|                 |                 | orientation of tool in IDA                      | 1            | ř           |            |             |
| th_pot(m)       | radian          | frame using joint                               | th_pot(m)    |             |            |             |
| <u>_</u> r - () |                 | potentiometer readings                          | 1.5014       |             |            |             |
|                 |                 | deflected location of tool                      |              |             |            |             |
| x_enc_defl(m)   |                 | as Cartesian coordinates                        | x_enc_defl(i | m) y_enc_d  | efl(m) z   | enc_defl(m) |
| y_enc_defl(m)   | meter           | in IDA frame using joint                        | 1.36         |             | 0.0032     | 0.497       |
| z_enc_defl(m)   |                 | encoder readings                                | -            |             |            |             |
| th enc defl(m)  |                 | deflected orientation of                        | hb d-69      | (\)         |            |             |
|                 | radian          | tool in IDA frame using                         | th_enc_defl  |             |            |             |
| ` ′             |                 | joint encoder readings                          | 1.50         | J14         |            |             |
|                 |                 | deflected location of tool                      |              |             |            |             |
| v. mot 1-fl/ )  |                 | as Cartesian coordinates                        | x_pot_defl(r | n) y_pot_de | efl(m) z_  | pot_defl(m) |
| x_pot_defl(m)   | *** a 4 - ··    | •   |              |             |            |             |
| y_pot_defl(m)   | meter           | in IDA frame using joint                        | 1.35         | 571         | 0.0016     | 0.5068      |
|                 | meter           | in IDA frame using joint potentiometer readings | 1.35         | 571         | 0.0016     | 0.5068      |
| y_pot_defl(m)   | meter<br>radian |   | th_pot_defl( |             | 0.0016     | 0.5068      |

|  |                       | joint potentiometer readings        |                       |                      |                       |                     |
|--|-----------------------|-------------------------------------|-----------------------|----------------------|-----------------------|---------------------|
| v1(rad/s)<br>v2(rad/s)<br>v3(rad/s)<br>v4(rad/s) | radians per<br>second | joint velocity [RA_DOF]             | v1(rad/s)<br>0.0024   | v2(rad/s)<br>0.0006  | v3(rad/s)<br>0.001    | v4(rad/s)<br>0.0025 |
| tau1(N-m)<br>tau2(N-m)<br>tau3(N-m)<br>tau4(N-m) | Newton<br>meter       | joint torque [RA_DOF]               | tau1(N-m)             | tau2(N-m)<br>14.5451 | tau3(N-m)<br>-41.0253 | tau4(N-m)<br>0      |
| Fr(N)<br>Ft(N)<br>Fz(N)                          | Newton                | end-effector force in tool<br>frame | Fr(N)<br>-3.6661      | Ft(N)<br>-0.7414     | Fz(N)<br>-0.0603      |                     |
| htr_cur(mA)                                      | milliampere           | sum of heater currents              | htr_cur(mA)<br>0.0015 |                      |                       |                     |
| grapple_phase                                    | n/a                   | grapple phase (Table 15)            | grapple_pha           | se                   |                       |                     |

In Table 12, the computed motor rotor temperatures  $T_R$  (trotor1(C), trotor2(C), trotor3(C), trotor4(C)) are obtained

from the motor case temperature  $T_C$  (tcase1(C), tcase2(C), tcase3(C), tcase4(C)) using a thermal model. The IDA MC measures each motor case temperature  $T_C$  (tcase1(C), tcase2(C), tcase3(C), tcase4(C)) and reports them to the IDA FSW as part of the IDA sensor data response message. At each timestep, the IDA FSW computes each motor rotor temperature  $T_R$  (trotor1(C), trotor2(C), trotor3(C), trotor4(C)) using the thermal model described below.

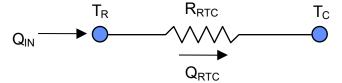


Figure 8 - Motor Temperature Model

$$Q_{IN} = I^2 R + I_{NL} V$$

$$Q_{RTC} = (T_R - T_C) R_{RTC}$$

$$R = R_{20C} (1 + T_{COEFF} (T_R - T_{CAL}))$$

$$T_R + = (Q_{IN} - Q_{RTC}) * \Delta t * (CM_R)$$

#### Where

 $Q_{IN}$  is the heat load on the rotor,

*I* is the motor current in amps which is converted by the FSW software from the raw digital number value by the following formula:  $I = I_M * I_H - I_B$ 

where  $I_M$  is the joint motor current slope,

 $I_H$  is the joint measured raw value,

 $I_B$  is the joint motor current offset (LSBs), current reference value when the joint angle is zero,

R is the rotor resistance in ohms,

*I*<sub>NL</sub> is the no-load current in amps,

 $T_R$  is the joint rotor temperature in Celsius,

 $T_C$  is the joint case temperature in Celsius,

V is the motor voltage in volts,

 $R_{RTC}$  is 1/(rotor-to-case thermal resistance) in watts/Celsius,

 $R_{20C}$  is the rotor resistance at 20°C in ohms,

 $T_{COEFF}$  is the temperature coefficient of resistance of copper in ohms/Celsius,

 $T_{CAL}$  is the calibration temperature in Celsius,

 $\Delta t$  is the actuator control loop rate in seconds (nominally 10Hz),

*CM<sub>R</sub>* is the rotor thermal mass in Joules/Celsius,

+= is treated as the C programming assignment operator.

The parameter values of the thermal model are found in the IDA Parameters files RA\_JOINT\_PARAMS (section Error! Reference source not found.) and RA\_THERMAL section 5.1.3.29).

The stat value is a word of 32 bits, which are described in Table 13. The bits are grouped in fours to represent the IDA 4 degrees of freedom. In each group of four bits, the very right bit corresponds to joint 1 (azimuth), the second to right bit to joint 2 (elevation), the third to right bit to joint 3 (elbow), and the very left bit to joint 4 (wrist).

The deflected location and orientation of tool as Cartesian coordinates in IDA frame using joint encoder readings (x\_enc\_defl(m), y\_enc\_defl(m), z\_enc\_defl(m), th\_enc\_defl(m)) and using joint potentiometer readings (x\_pot\_defl(m), y\_pot\_defl(m), z\_pot\_defl(m), th\_pot\_defl(m)) are obtained from, respectively, the location of tool using joint encoder readings (x\_enc(m), y\_enc(m), z\_enc(m), th\_enc(m)) and using joint potentiometer readings (x\_pot(m), y\_pot(m), z\_pot(m), th\_pot(m)). Due to the stiffness and mass of the IDA, the links can deflect under their own weight and the weight of a grappled payload. The IDA FSW computes the expected deflection from an internal model of the IDA stiffness and mass properties, knowledge of the grappled science instrument payload, payload masses, and the relative direction and magnitude of gravity [10][11]...

The end-effector forces (Fr(N), Ft(N), Fz(N)) are estimated from the joint motor current (cur1(mA), cur2(mA), cur3(mA), cur4(mA)) in the selected tool frame **Error! Reference source not ound.** Fr(N) is the radial force, Ft(N) is the translational force that is perpendicular Fr(N), and Fz(N) is the vertical force. More details on the end effector forces model are provided in Appendix D.

0 1 **Bits Description** 0 - 3motor power off on 4-7 direction of rotation pos neg 8-11 motor over current no yes

Table 13 - Bit-mapped status word

| 12-15 | brake   | on  | off |
|-------|---------|-----|-----|
| 16-19 | heaters | off | on  |
| 20-31 | spares  | N/A | N/A |

Table 14 - Selected tool

| Number | Tool           |
|--------|----------------|
| 0      | Blade 1        |
| 1      | Blade 2        |
| 2      | Scoop          |
| 3      | IDC            |
| 4      | Wrist          |
| 5      | Grapple        |
| 6      | Grapple-Attach |
| 7      | SEIS           |
| 8      | WTS            |
| 9      | HP3            |

Table 15 - Grapple phase

| Number | <b>Grapple Phase</b> |
|--------|----------------------|
| 0      | Launch-Locked        |
| 1      | Stowed               |
| 2      | OK-To-Open           |
| 3      | SEIS-Grappled        |
| 4      | WTS-Grappled         |
| 5      | HP3-Grappled         |

## 5.1.6 Engineering/Science Low Priority (SciLo) Data

Science Low Priority data is non-channelized telemetry science data that is sent to the *low* priority APID (88). The data and data product are equivalent to Science High Priority.

## 5.1.7 RSVP Replay MP4

An IDA engineer will create a MPEG-4 video of RSVP for the IDA activities performed during the soil mechanics experiments from the saved images from an RSVP simulation. The command is:

ffmpeg -i {inputs}.png -vcodec libx264 -pix\_fmt yuv420p {output\_name}.mp4

The resulting MP4 video will have H.264 video codec with no audio.

## 5.2 Document Product Formats

Documents in InSight archives are provided as PDF/A (https://www.pdfa.org/publication/iso-19005-pdfa/) or as plain ASCII text if no special formatting is required. Figures that accompany documents may be provided as TIFF, GIF, JPEG, or PNG files.

## 5.3 PDS Label

IDA raw and calibrated products are archived at the PDS Geosciences Node using the PDS4 archive standard [1-4]. The products are grouped into collections and bundles as described in Section 4. Each product is assigned a unique Logical Identifier (LID) and is accompanied by a label containing the product metadata. Labels are written in XML (Extensible Markup Language) and conform to XML and PDS4 standards. An example of an IDA label is given in Appendix E.

# APPENDIX A – SUPPORT STAFF AND COGNIZANT PERSONS

**Table 16 - Archive Support Staff and Cognizant Persons** 

| IDA Team              |             |                                    |  |
|-----------------------|-------------|------------------------------------|--|
| Name                  | Affiliation | Email                              |  |
| Hallie Abarca         | JPL         | hallie.e.gengl@jpl.nasa.gov        |  |
| Eloise Marteau        | JPL         | eloise.marteau@jpl.nasa.gov        |  |
| Ashitey Trebi-Ollennu | JPL         | ashitey.trebi-ollennu@jpl.nasa.gov |  |
| Grace Lim             | JPL         | grace.lim@jpl.nasa.gov             |  |

| PDS Geosciences Node       |                       |                           |  |  |
|----------------------------|-----------------------|---------------------------|--|--|
| Name Affiliation Email     |                       |                           |  |  |
| Raymond Arvidson, director | Washington University | arvidson@wunder.wustl.edu |  |  |
| Edward Guinness            | Washington University | guinness@wustl.edu        |  |  |
| Susan Slavney              | Washington University | susan.slavney@wustl.edu   |  |  |

# APPENDIX B – IDA DENAVIT-HARTENBERG LINK FRAMES

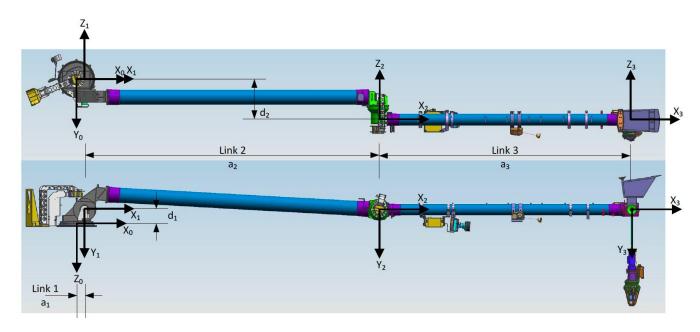


Figure 9 - Denavit-Hartenberg link frames

## APPENDIX C – STRUCTURE OF THE IDA SCIENCE BLOCK

The IDA flight software produces a number of different data blocks which reflect the IDA status during various phases of its operations. The IDA data which is useful for science investigation is organized in a data block which is generated by the IDA FSW at a regular frequency. These blocks are stored on-board and are downlinked later during a telemetry pass.

The structure is shown in C language syntax:

## APPENDIX D - END EFFECTOR FORCES MODEL

The end-effector forces model computes the radial force  $F_R$  and vertical force  $F_Z$  by solving the following system of equations:

$$c = \begin{bmatrix} F_R \\ F_Z \end{bmatrix} = A^{-1}b$$

where the vector *b* is given by:

$$\begin{aligned} b_{[0]} &= -m_3 p_3 (\ t_x \sin(q_1 + \ q_2 + \ q_3) - t_z \cos(q_1 + \ q_2 + \ q_3) \ ) - m_2 p_2 (\ t_x \sin(q_1 + \ q_2 + \ q_3) - t_z \cos(q_1 + \ q_2 + \ q_3) + a_2 \sin(q_1 + \ q_2) \ ) - m_1 p_1 (\ t_x \sin(q_1 + \ q_2 + \ q_3) - t_z \cos(q_1 + \ q_2 + \ q_3) + a_2 \sin(q_1 + \ q_2) + a_1 \sin(q_1) \ ) \\ b_{[1]} &= -m_3 p_3 (\ t_x \cos(q_1 + \ q_2 + \ q_3) + t_z \sin(q_1 + \ q_2 + \ q_3) + t_z \sin(q_1 + \ q_2 + \ q_3) + a_2 \cos(q_1 + \ q_2) \ ) + m_1 p_1 (\ t_x \cos(q_1 + \ q_2 + \ q_3) + t_z \sin(q_1 + \ q_2 + \ q_3) + a_2 \cos(q_1 + \ q_2) + a_1 \cos(q_1) \ ) \end{aligned}$$

and the matrix A is given by:

$$\begin{split} A_{[0][0]} &= p_3(\,t_x \sin(q_1 + q_2 + q_3) - t_z \cos(q_1 + q_2 + q_3)\,)^2 + p_2(\,t_x \sin(q_1 + q_2 + q_3) - t_z \cos(q_1 + q_2 + q_3) + a_2 \sin(q_1 + q_2)\,)^2 + p_1(\,t_x \sin(q_1 + q_2 + q_3) - t_z \cos(q_1 + q_2 + q_3) + a_2 \sin(q_1 + q_2) + a_1 \sin(q_1)\,)^2 \\ A_{[0][1]} &= -p_3(\,t_x \cos(q_1 + q_2 + q_3) + t_z \sin(q_1 + q_2 + q_3)\,)\,(\,t_x \sin(q_1 + q_2 + q_3) - t_z \cos(q_1 + q_2 + q_3)\,) - p_2(\,t_x \cos(q_1 + q_2 + q_3) + t_z \sin(q_1 + q_2 + q_3) + a_2 \cos(q_1 + q_2 + q_3) + a_2 \sin(q_1 + q_2 + q_3) + a_2 \cos(q_1 + q_2 + q_3$$

where:

 $q_{[0-3]}$  are the joint encoder values from SciHi Data enc1(rad), enc2(rad), enc3(rad), enc4(rad)) in Table 12,

 $p_{[0-3]}$  is the joint motor power (1.0 if on, 0.0 if off),

 $t_{\{x,y,z\}}$  is the wrist-to-tool vector found in **Error! Reference source not found.** A\_ARM\_PARAMS, tool from SciHi Data in Table 14

 $a_{[0-3]}$  are the joint link lengths found in **Error! Reference source not found.** A\_ARM\_PARAMS,

 $d_{\rm [0-3]}$  are the joint link offsets found in Error! Reference source not found. A\_ARM\_PARAMS,

 $m_{[0-3]}$  are the joint moments with gravity considered which is obtained as follows:

$$\begin{aligned} m_i &= tau_i + moment_{iz} \\ tau_i &= mtr\_torq\_sign_i * (mtr_{current_i} - cur_{no_{load_i}}) * Ka_i \end{aligned}$$

where:

 $moment_{iz}$  is the z-component of moment at the RA frames of joint i,  $mtr\_torq\_sign = \{-1.0, 1.0, 1.0, 1.0\}$ ,  $mtr_{current_i}$  is the motor current of joint i,  $cur_{no_{load_i}}$  is the no-load current for each joint as a function of temperature,  $Ka_i$  is the torque constant for each actuator as a function of temperature

The transverse force  $F_T$  is obtained from:

$$F_T = \frac{\left(F_R(d_1 + t_y) + m_0\right)}{\left(a_2\cos(q_1 + q_2) + a_1\cos(q_1) + a_0 + t_x\cos(q_1 + q_2 + q_3) + t_z\sin(q_1 + q_2 + q_3)\right)}$$

## APPENDIX E – EXAMPLE PDS LABEL FOR AN IDA DATA PRODUCT

```
<?xml version="1.0" encoding="UTF-8" standalone="no"?>
<?xml-model href="http://pds.nasa.gov/pds4/pds/v1/PDS4 PDS 1B10.sch"</pre>
  schematypens="http://purl.oclc.org/dsdl/schematron"?>
<?xml-model href="http://pds.nasa.gov/pds4/msn/v1/PDS4 MSN 1B00 1100.sch"</pre>
 schematypens="http://purl.oclc.org/dsdl/schematron"?>
<Product Observational xmlns="http://pds.nasa.gov/pds4/pds/v1"</pre>
    xmlns:msn="http://pds.nasa.gov/pds4/msn/v1"
    xmlns:pds="http://pds.nasa.gov/pds4/pds/v1"
    xmlns:xsi="http://www.w3.org/2001/XMLSchema-instance"
    xsi:schemaLocation="http://pds.nasa.gov/pds4/pds/v1
https://pds.nasa.gov/pds4/pds/v1/PDS4 PDS 1B10.xsd http://pds.nasa.gov/pds4/msn/v1
http://pds.nasa.gov/pds4/msn/v1/PDS4 MSN 1B00 1100.xsd">
  <Identification Area>
<logical identifier>urn:nasa:pds:insight ida:data raw calibrated:a0087 0209 615088547
615088547 190629192905 eu</legical identifier>
    <version id>1.0</version id>
    <title>IDA Science High Data Product</title>
    <information_model_version>1.11.1.0</information model version>
    cproduct class>Product Observational
    <Citation Information>
      <publication year>2019</publication year>
      <description>IDA Science High Data Product</description>
    </Citation Information>
  </Identification Area>
  <Observation Area>
    <Time Coordinates>
      <start date time>2019-06-29T13:56:40.702Z</start date time>
      <stop date time>2019-06-29T13:56:40.702Z</stop date time>
    </Time Coordinates>
    <Investigation Area>
      <name>InSight</name>
      <type>Mission</type>
      <Internal Reference>
<lid reference>urn:nasa:pds:context:investigation:mission.insight/lid reference>
        <reference_type>data_to_investigation</reference_type>
        <comment>This is the PDS4 logical identifier for the InSight
mission.</comment>
      </Internal Reference>
    </Investigation Area>
    <Observing System>
      <Observing System Component>
       <name>InSight Lander
       <type>Spacecraft</type>
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